

**SERVICING & STORMWATER MANAGEMENT
IMPLEMENTATION REPORT**

EDGEWOOD COMMERCIAL

**TOWNSHIP OF SOUTHGATE
VILLAGE OF DUNDALK**

PREPARED FOR:

FLATO DUNDALK MEADOWS INC.

PREPARED BY:

**C.F. CROZIER & ASSOCIATES INC.
1 FIRST STREET, SUITE 200
COLLINGWOOD, ON L9Y 1A1**

JANUARY 2023

CFCA FILE NO. 1060-5384

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TABLE OF CONTENTS

1.0	INTRODUCTION	1
2.0	SITE DESCRIPTION.....	1
3.0	PROPOSED DEVELOPMENT	2
4.0	PROPOSED SERVICING STRATEGY	2
4.1	Sanitary Servicing.....	2
4.2	Water Servicing.....	2
4.3	Utility Servicing.....	3
5.0	STORMWATER MANAGEMENT & SITE DRAINAGE	3
5.1	Design Criteria	3
5.2	Pre-Development Drainage Conditions	4
5.3	Proposed Drainage Conditions	4
5.4	Stormwater Quality Control.....	4
6.0	EROSION & SEDIMENTATION CONTROLS DURING CONSTRUCTION.....	5
7.0	CONCLUSIONS & RECOMMENDATIONS.....	5

LIST OF TABLES

Table 1: Edgewood Greens Development Details and Status

LIST OF APPENDICES

- Appendix A:** Water & Wastewater Capacity Calculations
- Appendix B:** Sanitary Sewer Design Sheet
- Appendix C:** Fire Flow Calculations
- Appendix D:** Storm Sewer Design Sheet

LIST OF FIGURES & DRAWINGS

- Figure 1:** Site Location Plan
- Figure 2:** Flato East Draft Plan
- Figure 3:** Edgewood Greens Composite Phasing Plan
- Figure 4:** Concept Site Plan
- Figure 5:** Pre-Development Drainage Plan
- Drawing C101:** General Servicing Plan
- Drawing C102:** General Grading Plan
- Drawing C103:** Erosion and Sediment Control Plan
- Drawing C104:** Construction Staging Plan
- Drawing C109:** Sanitary Drainage Plan (Edgewood Greens - Phase 11)
- Drawing C110:** Storm Drainage Plan (Edgewood Greens - Phase 11)

1.0 Introduction

C.F. Crozier & Associates Inc. (Crozier) has been retained by Flato Developments Inc. (Developer) to complete a Servicing and Stormwater Management Implementation Report and engineering design to support the Site Plan Application for a proposed commercial development known as Edgewood Commercial, referred to in this report as the Subject Development.

The Subject Development is located within the Draft Plan Approved Dundalk Meadows East Subdivision, herein referred to as Flato East. The general location of the Subject Development is shown on **Figure 1**.

2.0 Site Description

The 70 ha Flato Edgewood Greens Development in the southeast end of the Village of Dundalk is comprised of three Draft Plan Approved subdivisions:

- Dundalk Meadows West
- Dundalk Meadows East
- Dundalk Meadows North

The Subject Development is located within the Edgewood Greens Development, which is bounded by the Flato Meadows North Development to the north, Highway 10 to the east, open space to the south, and the Dundalk Meadows West Development to the west. Dundalk Meadows East is legally described as Part of Lot 233 and Lot 234, Concession 1, Village of Dundalk, Township of Southgate, County of Grey. The Dundalk Meadows East Draft Plan is shown in **Figure 2**.

The Edgewood Greens Development is being built out in phases. The boundaries of each of the phases within Edgewood Greens is shown in **Figure 3** and for additional information **Table 1** details the individual developments, their legal description, and their approval/design status.

Table 1: Edgewood Greens Development Details and Status

Development Property	Area (ha)	Units	Legal Description ⁽¹⁾	Phase of Development	Approval/Design Status
Dundalk Meadows West	13.1	70	Lot 18 and Part of Lots 17 and 21, Block P, Registered Plan 480 and Part of Lot 233 Concession 2	1	Built-Out
Dundalk Meadows East	40.2	471	Part of Lot 233 and Lot 234, Concession 1	2B	Built-Out
				7, 8 & 10	Draft Plan Approved/ Under Construction
				11	Draft Plan Approved/ Under Construction
				9	Draft Plan Approved/ Detailed Design
Dundalk Meadows North	16.2	267	Part of Lots 232, Concession 1	2A, 3-6	Built-Out

⁽¹⁾ Legal descriptions for all developments include "Village of Dundalk, Township of Southgate, County of Grey"

Within the Flato East Subdivision, the Subject Development is bounded by future Milliner Avenue to the south, future Symington Street to the west, future Colgan Crescent to the north, and Highway 10 to the east.

Geotechnical analysis determined that the site is underlain by Parkhill Loam, a medium textured soil derived from dolomitic limestone till, and Listowel Silt Loam, which carries the same characteristics as the Parkhill Loam. (Soil Survey of Grey County, 1979). Both soils are known to have poor drainage and are classified within the hydrologic soil group BC (Ministry of Transportation, 1997).

3.0 Proposed Development

The Subject Development is approximately 0.52 ha and is comprised of one single-story restaurant building with a gross floor area (GFA) of 454.1 square meters that can accommodate 90 seats. The development also includes 2 drive lane entrances and a 24-hour drive thru. The Subject Development also includes stormwater management, water, sanitary, typical utility, and site lighting infrastructure. The proposed Site Plan can be seen in **Figure 4**.

4.0 Proposed Servicing Strategy

4.1 Sanitary Servicing

As per the Township of Southgate “2022 Reserve Capacity” the existing wastewater treatment plant has an uncommitted reserve capacity of 182 new development equivalent residential units (ERUs). As of September 2022, allocation to service 29 ERUs required for the commercial block was granted by the Township of Southgate. For further information of the reserve capacities and summary of ERUs refer to **Appendix A** for relevant calculations.

Upon completion of Phase 11 of Edgewood Greens Subdivision, municipal gravity sanitary sewers will be available adjacent to the Subject Development with a 200 mm diameter service stub and maintenance hole constructed on the southwestern limit of the site along future Milliner Avenue. Refer to **Drawing C101** for location of the service stub and sanitary maintenance hole. The Sanitary Drainage Plan for Edgewood Greens - Phase 11 is shown in **Drawing C109**. It is anticipated that this servicing work will be complete and operational by June 2023.

Sanitary servicing within the proposed commercial building is to be provided by a 150 mm diameter internal sanitary sewer, connecting the building’s internal plumbing systems to the 200 mm diameter sanitary on Milliner Avenue.

Sanitary sewage discharge from the commercial block will flow west to the sanitary pumping station (SPS) located on VanDusen Avenue. From the SPS a forcemain discharges wastewater into SANMH#11A located on Moody Street. Gravity sewers along Moody, Elm and Hagan Streets convey the wastewater into the trunk sanitary sewer on Young Street, which subsequently discharges to the Town’s wastewater treatment plant. The existing Town sanitary sewer network has been evaluated by the Town’s Engineer and has capacity to convey sanitary flows from the entire Edgewood Greens Development. Refer to **Appendix B** for the Sanitary Sewer Design Sheet.

4.2 Water Servicing

The Subject Development will connect to the Town’s water distribution system via the 150mm dia. watermain service stub located off of Colgan Court. From this 150 mm dia. service the watermain will connect to the building via a split connection with one for domestic use and the other for fire protection. Watermain layout and connections are shown in **Drawing C101**.

The Township of Southgate within their "2022 Reserve Capacity" analysis determined the Township's water supply system has an available uncommitted reserve capacity of 1,999 units. Based on the analysis the Township has sufficient water supply to service the proposed development. Refer to **Appendix B** for relevant capacity calculations.

Fire flow requirements and available flows for the Commercial Block have been examined by Triton Engineering Services Limited (TESL), in conjunction with Crozier. Refer to **Appendix C** for the TESL Flato East (Edgewood Greens) Phases 7-11 Available Water Service Memorandum. TESL examined various scenarios for the expected maximum and minimum available pressure and fire flow within the bounds of the Subject Development. It is understood that the proposed Highway 10 connection will be completed in conjunction with Phase 11 of Dundalk Meadows East, and the proposed water tower is under construction. As such, it is anticipated that the proposed Water Tower will take place before the Subject Development is open. Therefore, the available fire flows per the Scenario #5 condition (Water Tower and Highway 10 connection – Refer to **Appendix C**) has been compared against the required fire flows. The proposed water distribution system will meet the fire flow requirements per the Office of the Fire Marshall – Fire Protection Water Supply Guideline for Part 3 in the OBC (2006) methodology for a commercial development. This is based on TESL Flato East (Edgewood Greens) Phases 7-11 Available Water Service Memorandum water distribution analysis scenario:

- Scenario #5 Condition – Dundalk Water Tower in operation, Highway 10 connection, and Phase 11 buildout.

Preliminary fire flows required to service the Commercial Block were determined to be 66.7 L/s as per the Fire Underwriters Survey, and 60 L/s as per the Office of the Fire Marshal. Refer to **Appendix C** for fire flow demand calculations.

The Township has indicated that the watermain distribution network located in the privately held portions of the development will remain under private ownership and will not be assumed by the municipality.

4.3 Utility Servicing

Edgewood Commercial will be serviced with natural gas, telephone, cable, TV and hydro. Coordination will be required with utility companies to ensure that sufficient capacity will exist within future facilities along Morgan Avenue and/or Colgan Crescent.

5.0 Stormwater Management & Site Drainage

5.1 Design Criteria

The stormwater management features for this site have been designed to comply with the policies and standards of the various agencies including the Township of Southgate, Ministry of the Environment, Conservation, and Parks, and the Grand River Conservation Authority. The stormwater management strategies for the proposed development are listed below:

- Water Quantity Control
 - Control of the post development peak flows to pre-development levels for all storms up to and including the 100-year at the selected point of interest.
- Water Quality Control
 - 80% removal efficiency of total suspended solids per MECP "Enhanced Protection" requirements.

- Development Standard
 - Minor and major drainage system to convey frequent and infrequent rainfall and runoff events, respectively.

In meeting the applicable policies and standards of the aforementioned agencies, the development will also be required to meet the following criteria:

- Manage the internal stormwater by safely conveying peak flows to suitable outlets and provide the necessary water quality controls.
- Manage any external drainage entering the site by providing safe conveyance across the Subject Development.
- Ensuring the development lands are not susceptible to flood inundation during all storm events.

5.2 Pre-Development Drainage Conditions

The existing drainage patterns of the site have been reflected in the Pre-Development Drainage Plan presented in **Figure 5**. The topographic survey of the site indicates the site is generally raised in the middle and slopes to the east and west. As such, runoff currently sheet flows towards Highway 10 to the east, and towards the Foley Drain to the west. The Foley Drain then flows south ultimately discharging to the Grand River.

5.3 Proposed Drainage Conditions

The internal drainage system for the Subject Development will consist of surface catchbasins and storm sewers to collect and convey flows to the storm sewer stub located near the south entrance of the site at Milliner Avenue. The Storm Drainage Plan and Storm Sewer Design Sheet for Edgewood Greens Phase 11 is shown in **Drawing C110** and **Appendix D**, respectively. The primary drainage areas consist of the parking lot area and the building rooftop referred to as catchment 104 in **Drawing C110**. Runoff from the building rooftop will be directed into the storm sewer system using storm drains. The parking lot will be graded to direct minor storm event runoff towards the catchbasins that flow towards STMMH01. Due to grading constraints, catchment 104A sheet flows north towards a swale that conveys runoff to a catchbasin which connects to the Phase 11 storm sewer system through STM PLUG 1. The storm sewer system conveys flows generated from minor storm events up to and including the five-year design storms. For larger storms the Subject Development will have overland flow routes that direct flows towards both entrances at Milliner and Colgan Court where the right-of-way will safely convey flows towards SWM Facility #3. The overland flow routes are designed to convey the major design storm flows, up to and including the 100-year and the regional storm with a maximum allowable onsite pond level of 250mm. Refer to **Drawing C102** for site grading and overland flow routes.

5.4 Stormwater Quality Control

The water quality and erosion controls will be provided by SWM Facility #3 which is currently under construction and will accommodate and provide both stormwater quality and quantity control for the Subject Development. Refer to the Edgewood Greens - Phase 11 Servicing & Stormwater Management Implementation Report for detailed stormwater management calculations, provided under separate cover. The Grand River is the ultimate receiver from the Subject Lands; therefore, the development will incorporate measures to provide "enhanced protection" quality control (*Stormwater Management Planning and Design Manual*, Ministry of the Environment, 2003).

6.0 Erosion & Sedimentation Controls During Construction

Erosion and sediment controls will be implemented on-site prior to construction where required and as directed by the Developer and their site representative. See **Drawing C103** for the Erosion & Sediment Control Plan. The following controls are to be implemented:

- Stone Mud Mat
 - A mud mat will be installed to reduce the amount of mud tracking onto existing paved roadways during site servicing operations.
- Silt Fencing
 - Silt fencing will be constructed in accordance with GRCA's Typical Detail of Silt/Sediment Fence (BSD-23 Draft). It should be noted that additional silt fencing may be added based on field decisions by the Engineer and Developer prior to, during, and following earthworks operations.

7.0 Conclusions & Recommendations

The analysis presented above provides a comprehensive servicing and stormwater management assessment in support of the proposed Edgewood Commercial Block Site Plan Application.

- Stormwater management objectives for water quality control have been addressed in the design of the Edgewood Commercial Block. Quantity controls up to and including the 100-year storm will be provided.
- Sanitary services for the Edgewood Commercial Block will be provided by a service extension from the sewer along future Milliner Avenue. The Edgewood Greens – Phase 11 sewer system has adequate capacity for the Subject Development.
- An internal watermain system will be provided connecting the future Colgan Crescent watermain to the proposed commercial building. The proposed water distribution system will meet the fire flow requirements.
- Sediment and erosion controls as specified, will be effective in preventing and controlling sediment from migrating into nearby swales, ditches, and watercourses.

Given the above noted conclusions, we support the development of the subject lands from the perspective of engineering servicing and stormwater management requirements.

Respectfully submitted,

C.F. CROZIER & ASSOCIATES INC.



Dylan Emery, P.Eng.
Project Engineer

C.F. CROZIER & ASSOCIATES INC.



Justin L'Abbe, P.Eng.
Project Engineer

APPENDIX A

Water & Wastewater Capacity Calculations



Project: Edgewood Commercial
Project No.: 1060-5384
Date: 2023.01.11
By: AM
Check By: JL'A

Flato Commercial - Water Flow Requirements

Developed Site Area	0.52 ha
Number of Restaurant Seats	90 seats
Retail Floor Area	454.00 m ²
Potable Water Design Flows	
24 Hour Drive-Through Restaurant	200 L/seat-day
Retail	5 L/m ² -day
Total Potable Water Design Flows	
Average 24 Hour Drive-Through Restaurant Daily Flow	0.21 L/sec
Average Retail Daily Flow	0.03 L/sec
Max Day Peak Factor (per MOECC Design Guidelines 2008)	2.75
Max Day Demand 24 Hour Drive-Through Restaurant Flow	0.57 L/sec
Max Day Demand Retail Flow	0.07 L/sec
Peak Hour Factor (per MOECC Design Guidelines 2008)	4.13
Peak Hour 24 Hour Drive-Through Restaurant Flow	0.86 L/sec
Peak Hour Retail Flow	0.11 L/sec
Fire Flow Demand (FUS)	66.7 L/sec
Overall Design Flow	67.35 L/sec



Project: Edgewood Commercial
 Project No.: 1060-5384
 Date: 2023.01.11
 By: AM
 Check By: JL'A

Flato Commercial - Sanitary Flow Requirements

Developed Site Area	0.52 ha
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Land Use Summary

1) 24 Hour Restaurant	90 seats
2) Commercial	454.00 m ²

Unit Sewage flows

Shopping Centre (MOE Design Guidelines, 2017)	5 L/m ² -day
24 Hour Restaurant (Ontario Building Code, 2006)	200 L/seat-day
Commercial (MOE Design Guidelines, 2017)	28000 L/ha-day

Possible Design Flows

Commercial (MOE Design Guidelines, 2017)	14560 L/day	DESIGN FLOW
24 Hour Restaurant (Ontario Building Code, 2006) and Shopping Centre (MOE Design Guidelines, 2017)	20270 L/day	
Combined Average Daily Flow Rate	34.8 m ³ /day	

Therefore use a 20,270 L/day Design Flow

Equivalent 24 Hour Restaurant Residential Population	52 Persons
Equivalent Shopping Centre Restaurant Residential Population	7 Persons
Equivalent Residential Units	22 Residential Units
Infiltration (Clearview Township Engineering Standards, 2017)	0.23 L/s/ha

Total Design Sewage Flows

Infiltration/Inflow Commercial	0.12 L/s
24 Hour Restaurant Average Daily Commercial Flow	0.21 L/s
Shopping Centre Average Daily Commercial Flow	0.03 L/s
24 Hour Restaurant Commercial Peak Factor (Harmon Formula)	4.31
Shopping Centre Commercial Peak Factor (Harmon Formula)	4.43
Total 24 Hour Restaurant Peak Daily Flow	0.96 L/s
Total Shopping Centre Peak Daily Flow	0.18 L/s



Project: Edgewood Greens - Phase 11
 Project No.: 1060-5771
 Date: 18-Jan-23
 By: AM
 Check: JL'A

Dundalk Sanitary Capacity Evaluation

DESCRIPTION	MARCH 2022	POST WWTF UPGRADES	UNITS
Available Capacity	1,832	3,025	m ³ /day
Average Day Flow	1,165	1,165	m ³ /day
Reserve Capacity	667	1,860	m ³ /day
Serviced Households	1,144	1,144	ERUs
Persons Per New Equivalent Residential Unit (2017 DC Background Study)	2.66	2.66	Persons
Average New Development Per Capita Flow	0.35	0.35	m ³ /day
Equivalent Flow Per Residential Unit	0.931	0.931	m ³ /day
Additional ERUs that can be serviced	716	1997	ERUs
TOTAL EQUIVALENT RESIDENTIAL UNIT (ERU) SUMMARY OF OCCUPIED, COMMITTED AND UNCOMMITTED UNITS			
DEVELOPMENT	OCCUPIED UNITS 2021	COMMITTED UNITS	UNCOMMITTED UNITS
White Rose (Phase 1 & 2)	63	3	0
Flato North (Phase 2A)	72	0	0
Flato North (Phase 3)	42	4	0
Flato North (Phase 4)	22	0	0
Flato North (Phase 5)	10	49	0
Flato North (Phase 6)	68	48	0
Glenelg (Phase 1)	0	183	0
Flato West Block 75	0	56	0
Flato East (Phase 7, 8 & 10)	0	188	0
Flato East (Phase 11)	0	143	0
White Rose (Phase 3)	0	35	0
Edgewood Commercial	0	29	0
Infill Lots	3	3	0
TOTAL COMMITTED UNITS 2022		741	
White Rose (Phase 3)	0	0	53
Flato East (Phase 9)	0	0	47
Flato East (Phase 11)	0	0	55
Glenelg (Phase 2)	0	0	155
Edgewood Commercial	0	0	0
Glenelg (Phase 3)	0	0	459
TOTAL UNCOMMITTED UNITS			1218
Total Number of Available ERUs Upon Completion of WWTF Upgrades			1997
Total Projected ERUs of Reserve Capacity Available Upon Occupation of Committed Units			1256
Projected ERUs of Reserve Capacity Available Upon Occupation of The Above Uncommitted Units			38



CROZIER
CONSULTING ENGINEERS

Project: Edgewood Greens - Phase 11
Project No.: 1060-5771
Date: 18-Jan-23
By: AM
Check: JL'A

Dundalk Water System Capacity Evaluation

DESCRIPTION	2022	UNITS	
Available Capacity	2,817	m ³ /day	
Max Day Flow	941	m ³ /day	
Reserve Capacity	1,876	m ³ /day	
Serviced Households	1,299	ERUs	
Persons Per Existing Residential Unit (2016 Census Data)	2.6	Persons	
Maximum Day Per Capita Flow	0.279	m ³ /day	
Persons Per New Equivalent Residential Unit (2017 DC Background Study)	2.66	Persons	
Addditional population that can be served	6724	Persons	
Additional ERUs that can be served	2528	ERUs	
TOTAL EQUIVALENT RESIDENTIAL UNIT (ERU) SUMMARY OF OCCUPIED, COMMITTED AND UNCOMMITTED UNITS			
DEVELOPMENT	OCCUPIED UNITS 2021	COMMITTED UNITS	UNCOMMITTED UNITS
White Rose (Phase 1 & 2)	63	3	0
Flato North (Phase 2A)	72	0	0
Flato North (Phase 3)	42	4	0
Flato North (Phase 4)	22	0	0
Flato North (Phase 5)	10	49	0
Flato North (Phase 6)	20	48	0
Glenelg (Phase 1)	0	183	0
Flato West Block 75	0	56	0
Flato East (Phase 7, 8 & 10)	0	188	0
Flato East (Phase 11)	0	143	0
White Rose (Phase 3)	0	35	0
Edgewood Commercial	0	29	0
Infill Lots	3	3	0
TOTAL COMMITTED UNITS 2022		741	
White Rose (Phase 3)	0	0	53
Flato East (Phase 9)	0	0	47
Flato East (Phase 11)	0	0	55
Glenelg (Phase 2)	0	0	155
Glenelg (Phase 3)	0	0	459
TOTAL UNCOMMITTED UNITS			1218
Total Number of Available ERUs		2528	
Total Projected ERUs of Reserve Capacity Available Upon Occupation of Committed Units		1787	
Projected ERUs of Reserve Capacity Available Upon Occupation of The Above Uncommitted Units		569	



March 28, 2022

Township of Southgate
R.R. #1
185667 Grey Road 9
Dundalk, Ontario
N0C 1B0

ATTENTION: Jim Ellis,
Public Works Manager

RE: Township of Southgate
Dundalk Water Supply and
Sewage Treatment Systems
2022 Reserve Capacity Calculations
Our File: A4160(22)-R04

Dear Sir:

The attached tables outline the 2022 reserve capacity calculations for the water supply and sewage treatment systems in Dundalk. The reserve capacities have been calculated in accordance with Ministry of Environment and Conservation and Parks (MECP) guidelines. 251 new residential units were connected to and **232** occupied within the municipal systems of Dundalk in 2021.

Table 3 provides a summary of Committed Developments which include White Rose Phases 1 and 2, Flato Phases 2-8 and 10, Flato Glenelg Development Phase 1 and the Flato West Apartment Building, totalling **534** equivalent residential units (ERUs). As Committed Units, these ERUs will not come out of the Uncommitted Reserve Capacity figures indicated on Tables 1 and Table 2. Table 3 further outlines the various potential developments that have been granted Draft Plan Approval, or are being considered, however have not been granted allocation.

Water System:

The three (3) year average maximum day demand of the water system increased from 918m³/d to **941m³/d** over the past year. The 2022 uncommitted reserve capacity of the water system is **1,999 ERU**. This is based on the Townships' amount of water taking permitted by the Permit to Take Water and committed developments as outlined in Table 3. The Permit to Take Water, indicates an allowable water taking of 2,817m³/day.

Refer to Table 1 for additional information regarding water system reserve capacity calculations.



Sewage Treatment Facility:

Table 2 summarizes the sewage treatment reserve capacity calculations for 2022. The three-year annual average day flow increased from 1,127 m³/d to **1,165m³/d**. Despite an increase in the serviced population in 2021, the 2021 uncommitted reserve capacity for the sewage treatment facility has increased from 127 ERUs to **182** new development ERUs.

Refer to Table 2 for additional information regarding sewage treatment system reserve capacity calculations.

Extraneous Flow:

In conjunction with the reserve capacity calculations, we have completed a high-level assessment of the extraneous flows within the Dundalk sewage collection system. This assessment compares the precipitation, temperature, average day demand of water and the average day sewage flow measured at the WWTP on a monthly basis. The results indicate that the extraneous flows over and above the expected amount within a typical system is, on average, **367m³/day**, which equates to an estimated **395 ERUs**. The relationship between the wastewater flows, precipitation and temperature is indicative of a system that is subject to both groundwater infiltration, and direct inflow. This is based on peaking of wastewater flows noted during the spring melt (i.e., March) and correlation noted to times of high precipitation but lower groundwater levels (i.e., July). Sump pump connections are likely a significant contributor.

Recommendation:

Following Council's review and adoption of the attached report, we would recommend that a copy of the report be forwarded to the MECP District Office in Owen Sound and the Grey County Planning Department. We trust you will find the enclosed to be in order. Should you have any questions, please do not hesitate to contact this office.

Respectfully,
Triton Engineering Services Limited



Dustin Lyttle, P. Eng.

cc: Dave Milliner, Township of Southgate
Clinton Stredwick, Township of Southgate
Bev Fisher, Township of Southgate



TABLE 1
TOWNSHIP OF SOUTHGATE
2022 RESERVE CAPACITY
DUNDALK WATER SYSTEM

DESCRIPTION	2021
1 Available Capacity ¹	2,817
2 Max Day Flow (m ³ /d) ²	941
3 Reserve Capacity (m ³ /d) (1) - (2)	1,876
4 Serviced Occupied Households ³	1,299
5 Persons Per Existing Residential Unit (2016 Census Data)	2.60
6 Population Served (4) x (5)	3,377
7 Maximum Day Per Capita Flow (m ³ /d) (2) ÷ (6)	0.279
8 Additional Population that can be Served (3) ÷ (7)	6,737
9 Person Per New Equivalent Residential Unit (2017 DC Background Study)	2.66
10 Additional ERUs that can be served. (8) ÷ (9)	2,533
11 Committed Development ERUs (Table 3)	534
12 Uncommitted Reserve Capacity (ERUs) (10) - (11)	1,999
¹ Available Capacity is based on lesser of Firm Capacity or Permit to Take Water. Firm capacity is 2,819m ³ /day, PTTW is 2,817m ³ /d. Well Production is 4,780m ³ /day.	
² Max day flow is the average of the maximum day flows from 2019, 2020 and 2021 (913, 905 and 1,004m ³ /d respectively). 2020 and 2019 Maximum day flows have been adjusted to account for high demands during various infrastructure works.	
³ Serviced occupied households is 1,067 (2020) + 232 units occupied in 2021.	



TABLE 2
TOWNSHIP OF SOUTHGATE
2022 RESERVE CAPACITY
DUNDALK SEWAGE TREATMENT FACILITY

DESCRIPTION	2021
1 Design Capacity of Sewage Treatment Facility (m ³ /d)	1,832
2 Average Day Flow ¹ (m ³ /d) (Average of 2019, 2020 and 2021 Average Day Flows)	1,165
3 Reserve Capacity (m ³ /d) (1) - (2)	667
4 Average New Development Per Capita Flow ² (m ³ /d)	0.350
5 Additional Population that can be Served (3) ÷ (4)	1,906
6 Person Per Equivalent Residential Unit (2017 DC Background Study)	2.66
7 ERU Flow Rate (m ³ /d) (4) x (6)	0.931
8 Additional ERUs that can be Served (5) ÷ (6)	716
9 Committed Development ERUs (Table 3)	534
10 Uncommitted Reserve Capacity (ERUs) (7) - (8)	182
¹ Average of the average day flows in 2019, 2020 and 2021 (1,114m ³ /day, 1,161m ³ /day and 1,220m ³ /day respectively).	
² As determined by new development flow analysis supported by flow monitoring program.	



TABLE 3
TOWNSHIP OF SOUTHGATE
2022 RESERVE CAPACITY
SUMMARY OF DUNDALK DEVELOPMENTS

COMMITTED DEVELOPMENTS	TOTAL UNITS	UNITS OCCUPIED IN 2021	REMAINING UNITS AT END OF 2021
White Rose (Phase 1 & 2)	66	63	3
Flato North (Phase 2A)	72	72	0
Flato North (Phase 3)	46	42	4
Flato North (Phase 4)	22	22	0
Flato North (Phase 5)	59	10	49
Flato North (Phase 6)	68	20	48
Flato Glenelg (Phase 1)	183	0	183
Flato West Block 75 (Phase 2) Apartment Building ¹	56	0	56
Flato East (7, 8 & 10)	188	0	188
INFILL LOTS ²		3	3
SUB-TOTAL		232	534
TOTAL COMMITTED UNITS			534
UNCOMMITTED DEVELOPMENT (DRAFT PLAN APPROVED)	TOTAL UNITS		
White Rose (Phase 3)	88		
Flato East (Phase 9)	47		
Flato East (11)	193		
Glenelg (Phase 2)	155		
Dundalk Commercial	24		
SUB-TOTAL	507		

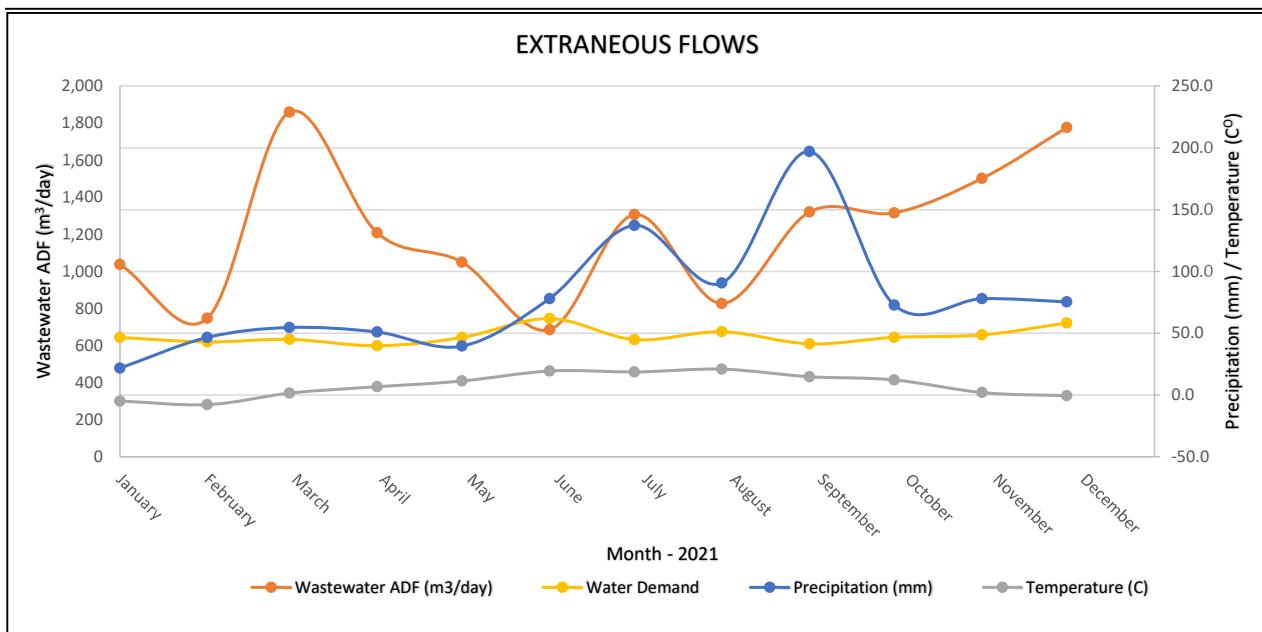
¹ Apartment units based on assumption that each unit is 0.7 ERU.

² 3 Infill Lots allocated annually.



TABLE 4
TOWNSHIP OF SOUTHGATE
2022 RESERVE CAPACITY
DUNDALK EXTRANEous FLOWS

MONTH	PRECIPITATION (mm) ⁴	AMBIENT TEMP. (C°) ⁴	WASTEWATER ADF (m ³ /day)	WATER ADD (m ³ /day)	EXTRANEous FLOW (m ³ /day) ¹
January-2021	21.6	-4.9	1,038	643	395
February-2021	46.6	-7.8	747	620	127
March-2021	54.6	1.4	1,860	633	1,227
April-2021	50.9	6.7	1,209	598	611
May-2021	39.5	11.2	1,050	643	407
June-2021	77.9	19.4	685	745	0
July-2021	137.2	18.7	1,306	632	674
August-2021	90.7	20.8	827	674	153
September-2021	196.9	14.7	1,320	609	711
October-2021	72.6	12.2	1,316	644	672
November-2021	77.9	1.9	1,501	657	844
December-2021	75.4	-0.7	1,776	722	1,054
AVERAGE			1,220	652	573
REASONABLE EXTRANEous FLOW BASED ON POPULATION(m³/day)²					203
EXTRANEous FLOW OVER AND ABOVE REASONABLE AMOUNT(m³/day)					370
EQUIVALENT RESIDENTIAL UNITS USED BY EXTRANEous FLOWS (ERU)³					398
¹ This is the Wastewater ADF minus the Water ADD, used to determine Sanitary Flow over and above expected.					
² Expected infiltration is 60 Litres per person per day based on modified historic MOE Standard.					
³ Based on New Development Equivalent Residential Unit Sanitary Flow Rate					
⁴ As recorded at Mount Forest Station.					



APPENDIX B

Sanitary Sewer Design Sheet

EDGEWOOD GREENS - PHASE 11

SANITARY SEWER DESIGN MODEL

DESIGN: JK/VP/AC/AM
 CHECK: DTE
 SUBMISSION: 4th Submission

N = 0.013
 Population = 3.5 p.p.u.
 Peak Factor (M) = $1 + (14/4 + [P/1000])^{0.5}$
 Avg. Daily/Capita Flow = 350 L/cap.d
 Q infiltration = 0.15 L/ha.s

Edgewood Greens Phase #	Catchment Area	FROM MH	TO MH	Length (m)	Inc. Area (Ha)	Cum. Area (Ha)	Lots	Inc. Pop	Total Trib Pop	Peak Factor	Avg. Flow (l/s)	Max Flow (l/s)	Infiltr. (l/s)	Total Infiltr.	Combined (l/s)	Pipe Diam (mm)	Upper Inv. El.	Lower Inv. El.	Slope (%)	Cap. (l/s)	Vel. (m/s)	q/Q	d/D	v/V	Act. Vel. m/s	Ground Upper	Ground Lower	Cover Upper	Cover Lower
7/8/10	1	EX. 11A	11B	29.00	0.35	0.35	6	21	21	4.38	0.09	0.37	0.05	0.05	0.42	200	513.73	513.06	2.30%	49.74	1.58	0.01	0.07	0.32	0.51	516.33	516.39	2.4	2.8
	1A	11B	3A	55.70	0.49	0.84	8	28	49	4.32	0.20	0.86	0.13	0.13	0.98	200	513.03	512.81	0.40%	20.74	0.66	0.05	0.15	0.52	0.34	516.39	516.15	3.2	2.8
	2	3A	3	84.65	0.48	1.32	7	25	74	4.28	0.30	1.27	0.07	0.20	1.47	200	512.79	512.45	0.40%	20.74	0.66	0.07	0.18	0.58	0.38	516.15	516.20	3.2	3.2
	3	1	2	37.90	0.43	0.43	7	25	25	4.37	0.10	0.43	0.06	0.06	0.50	200	512.79	512.04	2.00%	46.38	1.48	0.01	0.07	0.32	0.47	516.43	516.24	3.4	3.7
	4	2	3	43.40	0.35	0.78	5	18	42	4.33	0.17	0.74	0.05	0.12	0.85	200	512.01	511.84	0.40%	20.74	0.66	0.04	0.14	0.50	0.33	516.24	516.20	4.0	3.8
	5	3	4	57.53	0.54	2.64	7	25	140	4.20	0.57	2.38	0.08	0.40	2.78	200	511.82	511.59	0.40%	20.74	0.66	0.13	0.24	0.68	0.45	516.20	515.80	4.2	3.7
	6	4	5	57.50	0.60	3.24	9	32	172	4.17	0.69	2.90	0.09	0.49	3.38	200	511.57	511.34	0.40%	20.74	0.66	0.16	0.27	0.73	0.48	515.80	516.22	4.0	4.4
	7	5	6	20.90	0.30	3.54	3	11	182	4.16	0.74	3.07	0.05	0.53	3.60	200	511.29	511.21	0.40%	20.74	0.66	0.17	0.28	0.74	0.49	516.22	516.01	4.7	4.3
	8	6	7	62.10	0.19	3.73	1	4	186	4.16	0.75	3.13	0.03	0.56	3.69	200	511.16	510.91	0.40%	20.74	0.66	0.18	0.29	0.76	0.50	516.01	515.76	4.6	4.3
	9	7	8	98.00	0.50	4.23	6	21	207	4.14	0.84	3.47	0.08	0.63	4.10	200	510.89	510.50	0.40%	20.74	0.66	0.20	0.30	0.78	0.52	515.76	516.06	4.7	5.0
9	26	29	28	39.27	0.23	0.23	5	18	18	4.39	0.07	0.31	0.03	0.03	0.35	200	515.49	515.10	1.00%	32.80	1.04	0.01	0.07	0.32	0.33	518.09	518.83	2.4	3.2
	25	25	28	82.0	0.55	0.55	11	39	39	4.34	0.16	0.68	0.08	0.08	0.76	200	517.49	515.47	2.50%	51.86	1.65	0.01	0.07	0.32	0.53	520.63	518.83	2.9	2.8
	27	28	30	80.0	0.58	1.36	9	32	88	4.26	0.35	1.51	0.09	0.20	1.71	200	515.10	514.46	0.80%	29.34	0.93	0.06	0.16	0.54	0.50	518.83	517.80	3.5	2.8
	28	30	31	80.0	0.67	2.03	13	46	133	4.21	0.54	2.27	0.10	0.30	2.57	200	514.20	513.80	0.80%	29.34	0.93	0.09	0.20	0.62	0.58	517.80	516.87	3.4	2.6
	29	31	8	80.00	0.56	2.59	9	32	165	4.18	0.67	2.78	0.08	0.39	3.17	200	513.78	512.18	2.00%	46.38	1.48	0.07	0.18	0.58	0.86	516.87	516.06	2.9	3.4
7/8/10	10	8	9	65.50	0.53	7.35	9	32	403	4.02	1.63	6.56	0.08	1.10	7.66	200	510.48	510.22	0.40%	20.74	0.66	0.37	0.42	0.86	0.57	516.06	516.38	5.4	5.6
	11	9	10	20.90	0.25	7.60	3	11	413	4.02	1.67	6.72	0.04	1.14	7.86	200	510.17	510.08	0.40%	20.74	0.66	0.38	0.43	0.93	0.61	516.38	516.46	6.0	5.9
	12	10	11	67.30	0.56	8.16	9	32	445	4.00	1.80	7.20	0.08	1.22	8.43	200	510.03	509.76	0.40%	20.74	0.66	0.41	0.45	0.95	0.63	516.46	516.89	6.2	6.6
	20	25	24	80.0	0.45	0.45	12	42	42	4.33	0.17	0.74	0.07	0.07	0.80	200	517.57	515.97	2.00%	46.38	1.48	0.02	0.10	0.40	0.59	520.63	518.86	2.9	2.4
	19	24	11	80.0	0.59	1.04	16	56	98	4.25	0.40	1.69	0.09	0.16	1.84	200	513.97	513.43	0.70%	27.44	0.87	0.07	0.18	0.58	0.51	518.86	516.89	4.7	2.9
	13	11	12	74.62	0.33	9.53	6	21	564	3.95	2.28	9.01	0.05	1.43	10.44	250	509.68	509.46	0.30%	32.57	0.66	0.32	0.39	0.89	0.59	516.89	517.04	7.0	7.1
	14	12	13	74.62	0.44	9.97	9	32	595	3.93	2.41	9.48	0.07	1.50	10.98	250	509.44	509.21	0.30%	32.57	0.66	0.34	0.40	0.00	0.00	517.04	517.42	7.3	7.7

EDGEWOOD GREENS - PHASE 11 SANITARY SEWER DESIGN MODEL																													
DESIGN: JK/VP/AC/AM CHECK: DTE SUBMISSION: 4th Submission		N = 0.013 Population = 3.5 p.p.u. Peak Factor (M) = 1+(14/4+P/1000)^0.5 Avg. Daily/Capita Flow = 350 L/cap.d Q infiltration = 0.15 L/h.s Commercial Avg Flow 350 L/cap.d																											
Edgewood Greens Phase #	Catchment Area	FROM MH	TO MH	Length (m)	Inc. Area (Ha)	Cum. Area (Ha)	Lots	Inc. Pop	Total Trib Pop	Peak Factor	Avg. Flow (l/s)	Max Flow (l/s)	Infiltr. (l/s)	Total Infiltr.	Combined (l/s)	Pipe Diam (mm)	Upper Inv. El.	Lower Inv. El.	Slope (%)	Cap. (l/s)	Vel. (m/s)	q/Q	d/D	v/V	Act. Vel. m/s	Ground Upper	Ground Lower	Cover Upper	Cover Lower
11	1	15	16	75.00	0.22	0.22	8	28	28	4.36	0.11	0.49	0.03	0.03	0.53	200	515.49	514.72	1.00%	32.80	1.04	0.02	0.10	0.40	0.42	518.30	517.97	2.6	2.7
	13	01	16	10.00	0.52	0.74	N/A	59	59	4.30	0.24	1.03	0.08	0.11	1.14	200	514.85	514.80	0.50%	23.19	0.74	0.05	0.15	0.52	0.38	518.24	517.97	3.2	2.7
	2	16	17	39.30	0.10	1.06	2	7	94	4.25	0.38	1.62	0.02	0.16	1.78	200	514.72	514.52	0.50%	23.19	0.74	0.08	0.19	0.60	0.44	517.97	517.92	3.1	2.9
	11	42	17	79.00	0.47	0.47	14	49	49	4.32	0.20	0.86	0.07	0.07	0.93	200	515.35	514.56	1.00%	32.80	1.04	0.03	0.12	0.44	0.46	518.06	517.92	2.5	2.8
	3	17	18	80.00	0.23	1.76	7	25	168	4.18	0.68	2.83	0.03	0.26	3.10	200	514.48	514.08	0.50%	23.19	0.74	0.13	0.24	0.68	0.50	517.92	517.44	3.2	2.8
	9	43	18	74.00	0.50	0.50	18	63	63	4.29	0.26	1.10	0.08	0.08	1.17	200	514.87	514.13	1.00%	32.80	1.04	0.04	0.14	0.50	0.52	517.66	517.44	2.6	2.8
	4	18	19	67.80	0.19	2.45	7	25	255	4.11	1.03	4.24	0.03	0.37	4.61	200	514.05	513.72	0.50%	23.19	0.74	0.20	0.30	0.78	0.58	517.44	517.09	3.2	2.9
	5	19	20	20.20	0.07	2.52	4	14	269	4.10	1.09	4.47	0.01	0.38	4.84	200	513.67	513.56	0.50%	23.19	0.74	0.21	0.31	0.79	0.58	517.09	516.97	3.2	2.9
	6	20	21	73.90	0.41	2.93	14	49	318	4.07	1.29	5.24	0.06	0.44	5.68	200	513.51	513.14	0.50%	23.19	0.74	0.24	0.33	0.82	0.61	516.97	517.09	3.3	3.4
	7	21	22	70.00	0.36	3.29	10	35	353	4.05	1.43	5.79	0.05	0.49	6.28	200	513.11	512.06	1.50%	40.17	1.28	0.16	0.27	0.73	0.93	517.09	517.53	3.8	5.0
	12	41	40	22.00	0.21	0.21	7	25	25	4.37	0.10	0.43	0.03	0.03	0.47	200	515.55	515.33	1.00%	32.80	1.04	0.01	0.07	0.32	0.33	518.22	518.35	2.5	2.5
	14	40	38	59.00	0.43	0.64	15	53	77	4.27	0.31	1.33	0.06	0.10	1.43	200	515.30	515.01	0.50%	23.19	0.74	0.06	0.16	0.54	0.40	518.35	518.04	2.9	2.5
	15	32	36	26.60	0.19	0.19	6	21	21	4.38	0.09	0.37	0.03	0.03	0.40	200	515.83	515.56	1.00%	32.80	1.04	0.01	0.07	0.32	0.33	518.53	518.45	2.5	2.4
	16	36	37	16.60	0.13	0.32	2	7	28	4.36	0.11	0.49	0.02	0.05	0.54	200	515.51	515.35	1.00%	32.80	1.04	0.02	0.10	0.40	0.42	518.45	518.44	2.7	2.6
	17	37	38	68.30	0.33	0.65	10	35	63	4.29	0.26	1.10	0.05	0.10	1.19	200	515.30	514.96	0.50%	23.19	0.74	0.05	0.15	0.52	0.38	518.44	518.04	2.9	2.6
	18	38	39	80.00	0.37	1.66	7	25	165	4.18	0.67	2.78	0.06	0.25	3.03	200	514.88	514.48	0.50%	23.19	0.74	0.13	0.24	0.68	0.50	518.04	517.64	3.0	2.6
	12A	42	40	0.14	0.14	0	0	0	4.50	0.00	0.00	0.02	0.02	0.02	0.02	200	515.22	514.41	1.00%	32.80	1.04	0.04	0.14	0.50	0.52	518.06	517.64	2.6	2.7
	10	42	39	81.00	0.56	0.70	18	63	63	4.29	0.26	1.10	0.08	0.11	1.20	200	515.22	514.41	1.00%	32.80	1.04	0.04	0.14	0.50	0.52	518.06	517.64	2.6	2.7
	19	39	35	80.00	0.33	2.69	6	21	249	4.11	1.01	4.14	0.05	0.40	4.54	200	514.33	513.93	0.50%	23.19	0.74	0.20	0.30	0.78	0.58	517.64	517.56	3.1	3.1
	20	32	32A	50.00	0.24	0.24	7	25	25	4.37	0.10	0.43	0.04	0.04	0.47	200	515.56	515.06	1.00%	32.80	1.04	0.01	0.07	0.32	0.33	518.53	518.28	2.8	2.7
	20A	32A	33	60.00	0.36	0.60	10	35	60	4.30	0.24	1.04	0.05	0.09	1.13	200	515.03	514.73	0.50%	23.19	0.74	0.05	0.15	0.52	0.38	518.28	517.93	3.1	2.7
	21	33	33A	16.60	0.06	0.66	0	0	60	4.30	0.24	1.04	0.01	0.10	1.14	200	514.68	514.60	0.50%	23.19	0.74	0.05	0.15	0.52	0.38	517.93	517.82	3.1	2.7
	22	33A	35	68.30	0.16	0.82	3	11	70	4.28	0.28	1.21	0.02	0.12	1.34	200	514.55	514.21	0.50%	23.19	0.74	0.06	0.16	0.5					

APPENDIX C

Fire Flow Calculations

**Edgewood Commercial
Fire Protection Volume Calculation
CFCA File: 1060-5384**

2023.01.11

Page 1

**Water Supply for Public Fire Protection - 1999
Fire Underwriters Survey**

Part II - Guide for Determination of Required Fire Flow

1. An estimate of fire flow required for a given area may be determined by the formula:

$$F = 220 * C * \sqrt{A}$$

where

- F = the required fire flow in litres per minute
- C = coefficient related to the type of construction
 - = 1.5 for wood frame construction (structure essentially all combustible)
 - = 1.0 for ordinary construction (brick or other masonry walls, combustible floor and interior)
 - = 0.8 for non-combustible construction (unprotected metal structural components)
 - = 0.6 for fire-resistive construction (fully protected frame, floors, roof)
- A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building considered.

Proposed Buildings	Ordinary Construction
1 number of floors	0.8 C
454.1 sq.m. floor area	
100% Floor 1	
0% Floor 2	
0% Floor 3	
0% Floor 4	
454.1 sq.m. total floor area	

Therefore F= 4,000 L/min (rounded to nearest 1000 L/min)

Fire flow determined above shall not exceed:
 30,000 L/min for wood frame construction
 30,000 L/min for ordinary construction
 25,000 L/min for non-combustible construction
 25,000 L/min for fire-resistive construction

2. Values obtained in No. 1 may be reduced by as much as 25% for occupancies having low contents fire hazard or may be increased by up to 25% surcharge for occupancies having a high fire hazard.

Non-Combustible	-25%	Free Burning	15%
Limited Combustible	-15%	Rapid Burning	25%
Combustible	No Charge		

Low fire Hazard occupancy for dwellings	0% reduction
	0 L/min reduction

Therefore UPDATED F= 4,000 L/min (rounded to nearest 1000 L/min)

Note: Flow determined shall not be less than 2,000 L/min

3. Sprinklers - The value obtained in No. 2 above maybe reduce by up to 50% for complete automatic sprinkler protection.

Sprinkler System	Assume	30% reduction
		1,200 L/min reduction

Edgewood Commercial Fire Protection Volume Calculation CFCA File: 1060-5384

2023.01.11

Page 2

Water Supply for Public Fire Protection - 1999

Fire Underwriters Survey

Part II - Guide for Determination of Required Fire Flow

4. Exposure - To the value obtained in No. 2, a percentage should be added for structures exposed within 45 metres by the fire area under consideration. The percentage shall depend upon the height, area, and construction of the building(s) being exposed, the separation, openings in the exposed building(s), the length and height of exposure, the provision of automatic sprinklers and/or outside sprinklers in the building(s) exposed, the occupancy of the exposed building(s) and the effect of hillside locations on the possible spread of fire.

Separation	Charge	Separation	Charge
0 to 3 m	25%	20.1 to 30 m	10%
3.1 to 10 m	20%	30.1 to 45 m	5%
10.1 to 20 m	15%		

Exposed buildings

Exposed Buildings	Name	Distance	Percentage	Notes
	North	14	15%	600
	South	35	5%	200
	West	60	0%	0
	East		0%	0

800 L/min Surcharge

Determine Required Fire Flow

No. 1	4,000
No. 2	0 reduction
No. 3	1,200 reduction
No. 4	800 surcharge

Required Flow: 3,600 L/min
Rounded to nearest 1000L/min: 4,000 L/min

Required Duration of Fire Flow	
Flow Required L/min	Duration (hours)
2,000 or less	1.0
3,000	1.25
4,000	1.5
5,000	1.75
6,000	2.0
8,000	2.0
10,000	2.0
12,000	2.5
14,000	3.0
16,000	3.5
18,000	4.0
20,000	4.5
22,000	5.0
24,000	5.5
26,000	6.0
28,000	6.5
30,000	7.0
32,000	7.5
34,000	8.0
36,000	8.5
38,000	9.0
40,000 and over	9.5

Determine Required Fire Storage Volume

Flow from above 4,000 L/min

Required duration 1.50 hours

Therefore: 360,000 Litres or
360 cu.m. is the required fire storage volume.

**Edgewood Commercial
Fire Protection Volume Calculation
CFCA File: 1060-5384**

2023.01.11

Page 3

**Fire Protection Water Supply Guideline
Part 3 of the Ontario Building Code (2006)**

$$Q = KV S_{TOT}$$

Q = minimum supply of water in litres (L)

K = water supply coefficient

V = total building volume in cubic metres

S_{TOT} = total of spatial coefficient values from property line exposures on all sides

K = 31.0 Group E building with combustible construction (Table 1)

V = 2043.45 $h = 4.5m$ $A = 454.1\text{sqm}$

S_{TOT} = 2 S_{TOT} Need Not Exceed 2.0

$$\mathbf{Q = 126693.9 \quad L}$$

Based on ranges listed in Table 2, the required minimum water supply flow rate is $3,600 \quad \mathbf{L/min}$

$60 \quad \mathbf{L/s}$



Memorandum

DATE: July 15, 2021
TO: Darrin Tone & Haley Birrell
FROM: Dustin Lytle & John Koolhaas
RE: Flato East (Edgewood Greens)
Phases 7-11
Available Water Service
FILE: A4167B & A4167F

Introduction:

This memo is intended to provide insight on the expected water system configuration, operating conditions and available flow within Phases 7-13 of the Edgewood Greens Subdivision.

The following estimates are based on the topographic and watermain design information presented in:

- Revision 5 of the Edgewood Greens Phases 7, 8 and 10 design drawings, dated May 27, 2021
- Revision 2 of the Edgewood Greens Phases 11-13 Preliminary Future Road Profiles, dated August 19, 2020
- Servicing and Stormwater Management Implementation Report, Flato East Commercial Block, dated November 2020 - Submission No. 1, prepared by C.F. Crozier & Associates Inc.

Note: The watermain crossing the Foley Drain on Morgan Ave. is to be 250mm diameter east of Van Dusen until Milliner Ave.

The watermain is to be sized as 150mm throughout Phases 7 to 13 except for the following locations:

Diameter (mm)	Location	From	To
200	Russel Street		
200	Morgan Avenue	Russel Street	Van Dusen Avenue
250	Morgan Avenue	Van Dusen Avenue	Milliner Avenue
200	Morgan Avenue	Milliner Avenue	Symington Street
200	Symington Street	Morgan Avenue	Milliner Avenue
250	Symington Street	Milliner Avenue	Block 369 Stub
200	Highway 10 and through Lots 230/231 (Servicing Block)	Existing Highway 10 stub	Colgan Crescent

Assessment:

The following assessment has been completed under eight scenarios as described below.

Scenario 1: Phase 7 – 11: Water Tower & HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 7 – 11** under the following arrangement:

- Build out up to Phase 11.
- 200mm diameter watermain connection on Highway 10 **is provided** from the existing stub through to Colgan Crescent. *The details of how this connection will be made through the sideyard and/or park block will be determined at a later date.*
- Proposed Water Tower **is** in operation.

Scenario 2: Phase 7 – 11: Water Tower – No HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 7 – 11** under the following arrangement:

- Build out up to Phase 11.
- 200mm diameter watermain connection on Highway 10 **is not provided** from the existing stub through to Colgan Crescent.
- Proposed Water Tower **is** in operation.

Scenario 3: Phase 7 – 11: No Water Tower – HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 7 – 11** under the following arrangement:

- Build out up to Phase 11.
- 200mm diameter watermain connection on Highway 10 **is provided** from the existing stub through to Colgan Crescent.
- Proposed Water Tower **not** in operation.

Scenario 4: Phase 7 – 11: No Water Tower – No HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 7 – 11** under the following arrangement:

- Build out up to Phase 11.
- 200mm diameter watermain connection on Highway 10 **is not provided**.
- Proposed Water Tower **not** in operation.

For the above scenarios under the arrangement of build out up to Phase 11, all watermain south of Morgan Avenue (i.e., within Phases 12 and 13) has been assumed to have not yet been constructed including Milliner Avenue, McAllister Street, Symington Street, Colgan Crescent (only the section south of Morgan), and the commercial development.

Scenario 5: Phases 12 & 13: Water Tower & HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 12 & 13** under the following arrangement:

- Complete build out of all phases.
- 200mm diameter watermain connection on Highway 10 **is provided** from the existing stub through to Colgan Crescent. *The details of how this connection will be made through the sideway and/or park block will be determined at a later date.*
- Proposed Water Tower **is** in operation.

Scenario 6: Phases 12 & 13: Water Tower & No HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 12 & 13** under the following arrangement:

- Complete build out of all phases.
- 200mm diameter watermain connection on Highway 10 **is not provided** from the existing stub through to Colgan Crescent. *The details of how this connection will be made through the sideway and/or park block will be determined at a later date.*
- Proposed Water Tower **is** in operation.

Scenario 7: Phases 12 & 13: No Water Tower & HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 12 & 13** under the following arrangement:

- Complete build out of all phases.
- 200mm diameter watermain connection on Highway 10 **is provided** from the existing stub through to Colgan Crescent.
- Proposed Water Tower **not** in operation.

Scenario 8: Phases 12 & 13: No Water Tower & No HWY 10 Connection

This scenario models the maximum and minimum expected available pressure and fire flow within the bounds of **Phases 12 & 13** under the following arrangement:

- Complete build out of all phases.
- 200mm diameter watermain connection on Highway 10 **is not provided**.
- Proposed Water Tower **not** in operation.

Results:

Note: all pressures and flows modelled are at the proposed road centre line elevation. Watermain placement and sizing has been assumed for developments where detailed design is not available.

Refer to attached Figure 1 for additional information.

Table 1: Phase 7 -11 Modelling Results (Scenarios 1 – 4)

Scenario	Pressure		Fire Flow	
	Maximum (PSI)	Minimum (PSI)	Maximum (L/s)	Minimum (L/s)
No.1: Tower & HWY 10 Connection	73 Russel-Wright intersection	67 Russel-Van Dusen intersection	222 Russel-Morgan intersection	156 West end of Moody Street at connection to Existing
No.2: Tower & No HWY 10 Connection	73 Russel-Wright Intersection	67 Russel-Van Dusen intersection	175 Russel-Morgan intersection	115 Colgan Crescent
No.3: No Water Tower & HWY 10 Connection	73 Russel-Wright Intersection	66 Russel-Van Dusen intersection	110 Russel-Morgan intersection	105 West end of Moody Street at connection to Existing
No.4: No Water Tower & No HWY 10 Connection	73 Russel-Wright intersection	66 Russel-Van Dusen intersection	109 Russel-Morgan intersection	89 Colgan Crescent

Table 2: Phase 11 – 13 Modelling Results (Scenarios 5 – 8)

Scenario	Pressure		Fire Flow	
	Maximum (PSI)	Minimum (PSI)	Maximum (L/S)	Minimum (L/S)
No.5: Tower & HWY 10 Connection	71 Milliner-Morgan Intersection	69 Commercial Development	205 Milliner-Morgan Intersection	112 Milliner Stub at HWY-10 Intersection
No.6: Tower & No HWY 10 Connection	71 Milliner-Morgan Intersection	69 Commercial Development	150 Milliner-Morgan Intersection	97 Milliner Stub at HWY-10 Intersection
No.7: No Water Tower & HWY 10 Connection	70 Milliner-Morgan Intersection	69 Commercial Development	101 Milliner-Morgan Intersection	82 Milliner Stub at HWY-10 Intersection
No.8: No Water Tower & No HWY 10 Connection	70 Milliner-Morgan Intersection	69 Commercial Development	97 Milliner-Morgan Intersection	76 Milliner Stub at HWY-10 Intersection

Any questions please contact us.

TOWNSHIP OF SOUTHGATE



DUNDALK EDGEWOOD GREENS SUBDIVISION

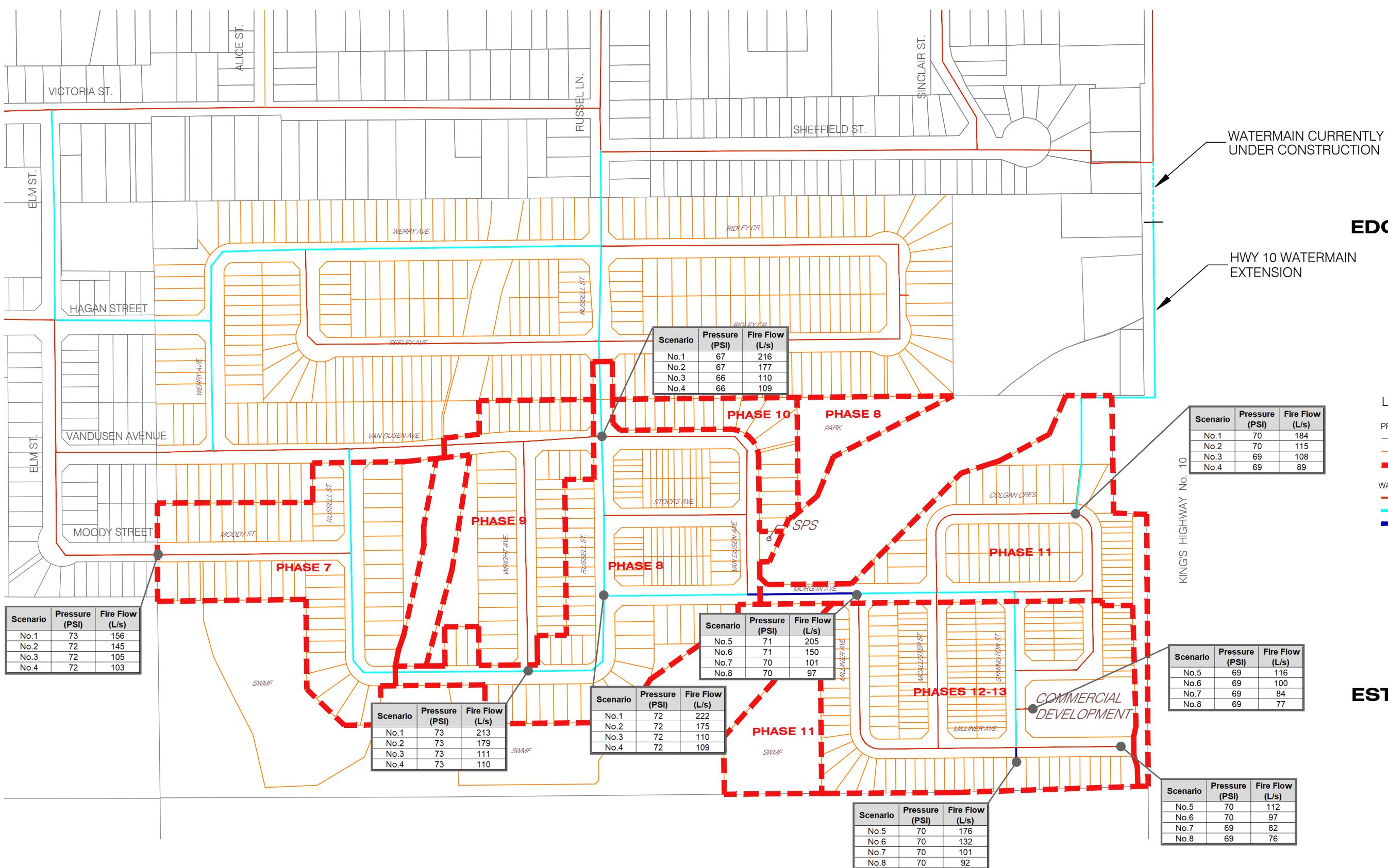


FIGURE 1

ESTIMATED AVAILABLE WATER SERVICE

JULY 2021

SCALE 1:4,000
A4167B

APPENDIX D

Storm Sewer Design Sheet

EDGEWOOD GREENS - PHASE 11

1060-5771
STORM SEWER DESIGN SHEET

FREQUENCY - 5 YEAR - MTO LOOKUP TOOL											
Coef. A=	30.6	Coef. B=	-0.699	Coef. C=							
FREQUENCY - 100 YEAR - MTO LOOKUP TOOL											
Coef. A=	51	Coef. B=	-0.69	Coef. C=							

MATERIAL	MANNINGS "n"	
	PVC	0.013
CONC.		0.013
CSP		0.024

DESIGNED BY: AM
CHECKED BY: DTE
DATE: 2023.01.18
ISSUED FOR: 4th Submission

CATCHMENT I.D.	STREET	FROM MH	TO MH	AREA (A) (Ha)	5 YEAR RUN-OFF COEFF (C ₅)	100 YEAR RUN-OFF COEFF (C ₁₀₀)	DESIGN STORM	A x C _s	5 YEAR CUMUL. A x C _s	100 YEAR CUMUL. A x C ₁₀₀	TIME OF CONC. (min.)	5 YEAR I (mm/hr)	100 YEAR I (mm/hr)	CONTROLLED FLOW (FOUNDATION SERVICES)	Q (RUNOFF) (l/sec)	DESIGN FLOW (l/sec)	PIPE SLOPE (%)	DIA. (mm)	MANNING'S "n"	VEL. (m/sec)	LENGTH (m)	TIME OF FLOW (min)	PIPE CAPACITY (l/sec)	PIPE INV ELEV. (m)	PIPE OVB ELEV. (m)	GROUND ELEV.		COVER				
																								UPPER END	LOWER END	UPPER END	LOWER END					
	Colgan Cr	CBMH8A	CBMH11	0.00	0	0.00	5 year	0.00	0.00	10.00	107.07	175.59	0.75	0.00	0.75	0.50%	300	0.013	0.97	60.5	1.04	68.38	1%	516.68	516.37	516.98	516.67	518.47	518.22	1.49	1.54	
139A	Colgan Cr	CB6	CBMH11	0.09	0.68	0.85	5 year	0.06	0.06	10.00	107.07	175.59	0.00	18.22	18.22	0.50%	300	0.013	0.97	8.0	0.14	68.38	27%	516.72	516.68	517.02	516.98	518.22	518.01	1.20	1.24	
139	Colgan Cr	CBMH11	CBMH22	0.12	0.68	0.85	5 year	0.08	0.14	11.04	99.90	163.98	1.28	39.66	40.93	0.50%	300	0.013	0.97	41.2	0.71	68.38	60%	516.35	516.15	516.65	516.45	518.22	518.01	1.56		
140A	Colgan Cr	CB8	CBMH22	0.07	0.68	0.85	5 year	0.05	0.05	0.00	10.00	107.07	175.59	0.00	14.17	14.17	0.50%	300	0.013	0.97	8.1	0.14	68.38	21%	516.51	516.47	516.81	516.77	518.01	518.01	1.20	1.24
141	Colgan Cr	RLCB16	CBMH22	0.11	0.53	0.66	5 year	0.06	0.06	10.00	107.07	175.59	0.00	17.35	17.35	0.50%	300	0.013	0.97	35.0	0.60	68.38	25%	516.33	516.15	516.63	516.45	517.96	518.01	1.33	1.56	
140	Colgan Cr	CBMH22	STMMH11	0.09	0.68	0.85	5 year	0.06	0.31	0.00	11.75	95.64	157.07	1.50	82.39	83.89	0.50%	375	0.013	1.12	20.7	0.31	123.98	68%	516.07	515.97	516.45	516.34	517.91	517.91	1.56	
142	Colgan Cr	CB7	CBMH13	0.06	0.68	0.85	5 year	0.04	0.04	0.00	10.00	107.07	175.59	0.00	12.14	12.14	0.50%	300	0.013	0.97	8.0	0.14	68.38	18%	515.86	515.82	516.16	516.12	517.71	517.71	1.55	1.59
142A	Colgan Cr	CBMH13	DCBMH7	0.10	0.53	0.66	5 year	0.05	0.40	0.00	12.43	91.99	151.15	1.65	103.24	104.89	0.50%	375	0.013	1.12	44.6	0.66	123.98	85%	515.75	515.52	516.12	515.90	517.71	517.35	1.59	
143	Colgan Cr	DCB7	DCBMH7	0.19	0.68	0.85	5 year	0.13	0.13	0.00	10.00	107.07	175.59	0.08	38.46	38.53	0.50%	300	0.013	0.97	8.0	0.14	68.38	56%	515.67	515.63	515.97	515.93	517.35	517.35	1.38	1.42
143A	Colgan Cr	DCBMH7	STMMH13	0.11	0.68	0.85	5 year	0.07	0.61	0.00	13.09	88.71	145.83	1.80	149.86	151.66	0.50%	450	0.013	1.27	18.0	0.24	201.60	75%	515.45	515.36	515.90	515.81	517.35	517.50	1.45	
	Colgan Cr	CBMH8A	STMMH9	0.00	0	0.00	5 year	0.00	0.00	0.00	10.00	107.07	175.59	0.08	0.00	0.08	0.50%	300	0.013	0.97	10.8	0.19	68.38	0%	516.76	516.71	517.06	517.01	518.47	518.43	1.41	1.42
	Colgan Cr	STMMH9	CBMH10B	0.00	0	0.00	5 year	0.00	0.00	0.00	10.19	105.70	173.37	0.30	0.00	0.30	0.50%	300	0.013	0.97	18.5	0.32	68.38	0%	516.63	516.53	516.93	516.83	518.43	518.26	1.50	1.43
127B	Colgan Cr	CB10	CBMH10B	0.12	0.68	0.85	5 year	0.08	0.08	0.00	10.00	107.07	175.59	0.00	24.29	24.29	0.50%	300	0.013	0.97	8.0	0.14	68.38	36%	516.75	516.71	517.05	517.01	517.36	518.26	0.31	1.25
127A	Colgan Cr	CBMH10B	CBMH10	0.06	0.68	0.85	5 year	0.04	0.12	0.00	10.51	103.44	169.72	0.30	35.20	35.50	0.50%	300	0.013	0.97	45.0	0.78	68.38	52%	516.48	516.26	516.78	516.56	518.26	518.04	1.48	
128C	Colgan Cr	RLCB17	RLCBMH8	0.03	0.53	0.66	5 year	0.02	0.02	0.00	10.00	107.07	175.59	0.23	4.73	4.96	0.50%	300	0.013	0.97	28.5	0.49	68.38	7%	517.07	516.93	517.37	517.23	518.85	518.89	1.49	1.66
128B	Colgan Cr	RLCBMH8	RLCBMH5	0.03	0.53	0.66	5 year	0.02	0.03	0.00	10.49	103.53	169.87	0.60																		

EDGEWOOD GREENS - PHASE 11

1060-5771
STORM SEWER DESIGN SHEET

FREQUENCY - 5 YEAR - MTO LOOKUP TOOL										
Coef. A=	30.6	Coef. B=	-0.699	Coef. C=						
FREQUENCY - 100 YEAR - MTO LOOKUP TOOL										
Coef. A=	51	Coef. B=	-0.69	Coef. C=						

FOUNDATION SERVICES FLOW (L/sec./lot) =
INITIAL TIME OF CONCENTRATION (minutes) =

0.075

10.00

MATERIAL	MANNINGS "n"
PVC	0.013
CONC.	0.013
CSP	0.024

DESIGNED BY: AM
CHECKED BY: DTE
DATE: 2023.01.18
ISUED FOR: 4th Submission

CATCHMENT I.D.	STREET	FROM MH	TO MH	5 YEAR RUN-OFF COEFF	100 YEAR RUN-OFF COEFF	DESIGN STORM	5 YEAR A x C	100 YEAR A x C ₁₀₀	TIME OF CONC.	5 YEAR I	100 YEAR I	CONTROLLED FLOW (FOUNDATION SERVICES)	Q (RUNOFF)	DESIGN FLOW	PIPE SLOPE	DIA.	MANNING'S "n"	VEL.	LENGTH	TIME OF FLOW	PIPE CAPACITY	CAPACITY (%)	PIPE INV ELEV.		PIPE OVB ELEV.		GROUND ELEV.		COVER			
																						UPPER END	LOWER END	UPPER END	LOWER END	UPPER END	LOWER END					
125 149+126	Milliner Ave	RLCBMH9	DCBMH10	0.09	0.53	0.66	5 year	0.05	0.07	0.00	10.24	105.33	172.78	0.23	20.18	20.40	2.00%	300	0.013	1.93	35.0	0.30	136.76	15%	515.68	514.98	515.98	515.28	517.18	516.83	1.20	1.55
	Milliner Ave	DCBMH10	DCBMH4	0.26	0.68	0.85	5 year	0.18	0.25	0.00	10.54	103.21	169.35	0.23	70.50	70.73	2.00%	300	0.013	1.93	9.3	0.08	136.76	52%	514.93	514.75	515.23	515.05	516.83	516.81	1.60	1.76
104A	Milliner Ave	STMPUG1	CBMH1A	0.08	0.25	0.31	5 year	0.02	0.02	0.00	10.00	107.07	175.59	0.00	5.95	5.95	0.40%	300	0.013	0.87	16.5	0.32	61.16	10%	516.40	516.33	516.70	516.63	516.71	518.22	0.01	1.59
	Milliner Ave	CBMH1A	CBMH1	0.00	0.00	0.00	5 year	0.00	0.02	0.00	10.32	104.75	171.84	0.30	5.82	6.12	0.50%	300	0.013	0.97	30.4	0.52	68.38	9%	516.33	516.18	516.63	516.48	518.22	518.07	1.59	1.59
101	Milliner Ave	CBMH1	CBMH2	0.05	0.68	0.85	5 year	0.03	0.05	0.00	10.84	101.18	166.06	0.60	15.19	15.79	0.50%	300	0.013	0.97	41.9	0.72	68.38	23%	516.16	515.95	516.46	516.25	518.07	517.87	1.61	1.62
110D	Milliner Ave	RLCB22	CBMH2	0.02	0.53	0.66	5 year	0.01	0.01	0.00	10.00	107.07	175.59	0.08	3.16	3.23	0.50%	300	0.013	0.97	14.7	0.25	68.38	5%	516.57	516.50	516.87	516.80	518.06	517.87	1.19	1.07
104	Milliner Ave	STMMH01	CBMH2	0.43	0.81	1.00	5 year	0.35	0.35	0.00	10.00	107.07	175.59	0.00	103.67	103.67	0.50%	450	0.013	1.27	14.0	0.18	201.60	51%	515.96	515.89	516.41	516.34	518.22	517.87	1.81	1.53
103	Milliner Ave	CBMH2	DCBMH1	0.07	0.68	0.85	5 year	0.05	0.46	0.00	11.56	96.73	158.84	0.75	123.83	124.58	0.50%	450	0.013	1.27	19.0	0.25	201.60	62%	515.80	515.70	516.25	516.15	517.87	517.76	1.62	1.61
107	Milliner Ave	DCB1	DCBMH1	0.11	0.68	0.85	5 year	0.07	0.07	0.00	10.00	107.07	175.59	0.00	22.26	22.26	2.00%	300	0.013	1.93	8.0	0.07	136.76	16%	516.12	515.96	516.42	516.26	517.76	517.76	1.34	1.50
106	Milliner Ave	DCBMH1	CBMH2A	0.06	0.68	0.85	5 year	0.04	0.58	0.00	11.81	95.29	156.51	0.83	152.61	153.44	0.50%	475	0.013	1.31	19.4	0.25	232.87	66%	515.68	515.58	516.15	516.05	517.76	517.82	1.61	1.77
109B	Colgan Cr	RLCB12A	CBMH9	0.04	0.53	0.66	5 year	0.02	0.02	0.00	10.00	107.07	175.59	0.15	6.31	6.46	0.50%	300	0.013	0.97	6.7	0.11	68.38	9%	516.66	516.63	516.96	516.93	518.33	517.94	1.36	1.01
110C	Colgan Cr	RLCB21	CBMH9A	0.02	0.53	0.66	5 year	0.01	0.01	0.00	10.00	107.07	175.59	0.08	3.16	3.23	0.50%	300	0.013	0.97	8.3	0.14	68.38	5%	516.76	516.72	517.06	517.02	518.12	517.94	1.06	0.92
109	Colgan Cr	CBMH9A	CBMH9	0.13	0.68	0.85	5 year	0.09	0.10	0.00	10.14	106.01	173.88	0.08	29.18	29.25	0.50%	300	0.013	0.97	8.0	0.14	68.38	43%	516.47	516.43	516.97	516.93	517.94	517.94	0.97	1.01
109A	Colgan Cr	CBMH9	DCBMH9A	0.07	0.53	0.66	5 year	0.04	0.16	0.00	10.28	105.01	172.26	0.38	45.92	46.30	0.50%	300	0.013	0.97	25.5	0.44	68.38	68%	516.55	516.42	516.85	516.72	517.94	517.82	1.09	1.09
110A	Colgan Cr	DCB9A	DCBMH9A	0.04	0.68	0.85	5 year	0.03	0.03	0.00	10.00	107.07	175.59	0.00	8.10	8.10	0.50%	300	0.013	0.97	8.0	0.14	68.38	12%	516.52	516.48	516.82	516.78	517.22	517.82	0.40	1.03
134B	Colgan Cr	DCBMH9A	CBMH4A	0.06	0.53	0.66	5 year	0.03	0.22	0.00	10.72	101.99	167.36	0.38	61.33	61.70	0.50%	300	0.013	0.97	18.0</											

EDGEWOOD GREENS - PHASE 11

1060-5771
STORM SEWER DESIGN SHEET

FREQUENCY - 5 YEAR - MTO LOOKUP TOOL									
Coef. A=	30.6	Coef. B=	-0.699	Coef. C=					
FREQUENCY - 100 YEAR - MTO LOOKUP TOOL									
Coef. A=	51	Coef. B=	-0.69	Coef. C=					

FOUNDATION SERVICES FLOW (L/sec/lot) =
INITIAL TIME OF CONCENTRATION (minutes) =0.075
10.00

MATERIAL	MANNINGS "n"
PVC	0.013
CONC.	0.013
CSP	0.024

DESIGNED BY: AM
 CHECKED BY: DTE
 DATE: 2023.01.18
 ISUED FOR: 4th Submission

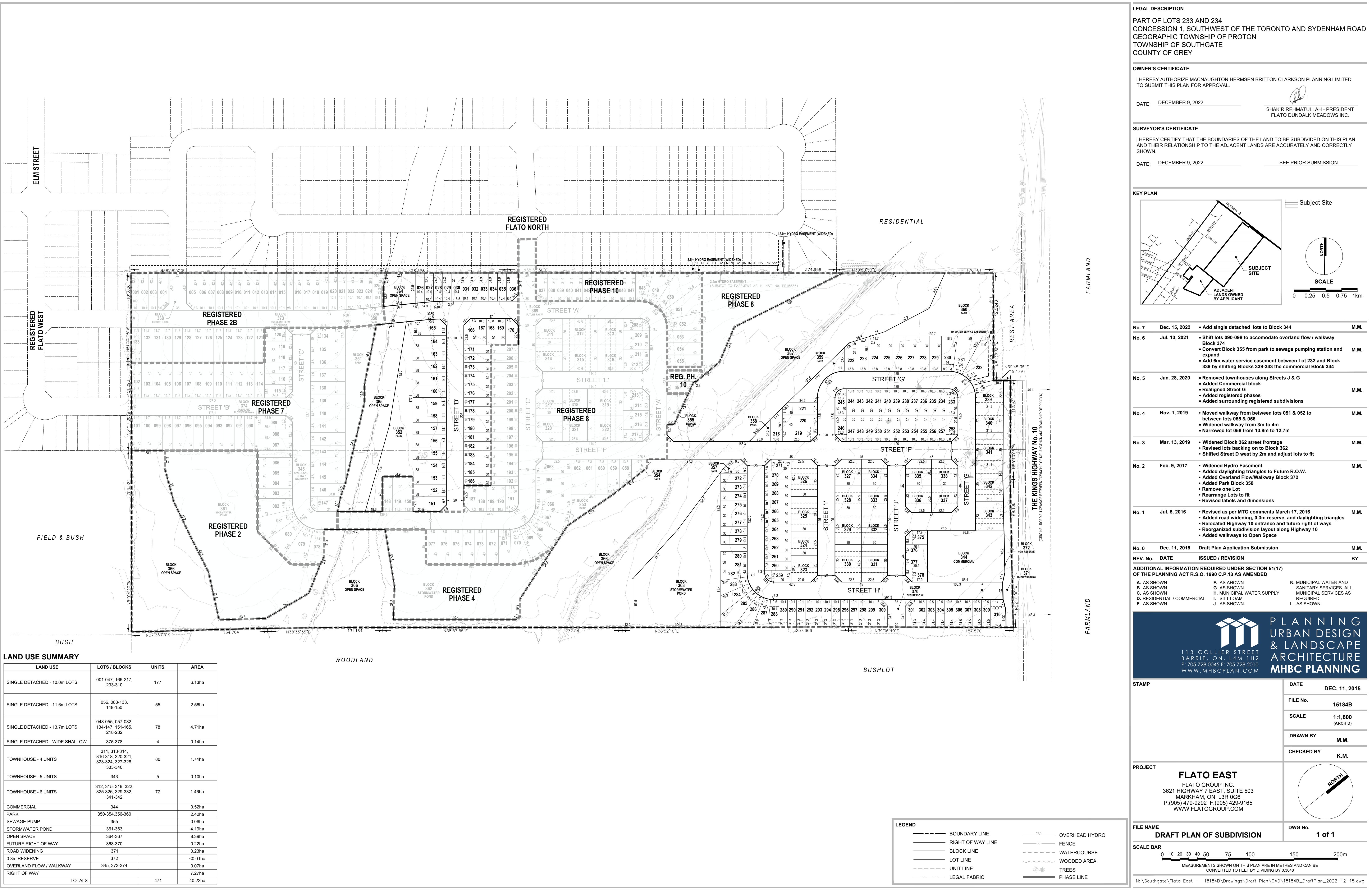
CATCHMENT I.D.	STREET	FROM MH	TO MH	5 YEAR RUN-OFF COEFF	100 YEAR RUN-OFF COEFF	DESIGN STORM	A x C	CUMUL.	100 YEAR TIME OF CONC.	5 YEAR I	100 YEAR I	CONTROLLED FLOW (FOUNDATION SERVICES)	Q (RUNOFF)	DESIGN FLOW	PIPE SLOPE	DIA.	MANNING'S "n"	VEL.	LENGTH	TIME OF FLOW	PIPE CAPACITY	PIPE CAPACITY (%)	PIPE INV ELEV.		PIPE OVB ELEV.		GROUND ELEV.		COVER			
																						UPPER END	LOWER END	UPPER END	LOWER END	UPPER END	LOWER END	UPPER END	LOWER END			
																						END	END	END	END	END	END					
146A	Morgan Ave	DCB12	FOLEY	0.08	0.68	0.85	5 year	0.05	0.05	0.00	10.00	107.07	175.59	0.00	16.19	16.19	0.50%	300	0.013	0.97	21.0	0.36	68.38	24%	515.32	515.21	515.62	515.51	517.12	N/A	1.51	N/A
100	South East Rear Lots	RLCB01A	RLCBMH02A	0.09	0.6	0.75	100 year	0.07	0.00	0.07	10.00	107.07	175.59	0.00	32.95	32.95	0.30%	300	0.013	0.75	20.9	0.47	52.97	62%	514.55	514.49	514.85	514.79	515.78	516.42	0.93	1.63
100A	South East Rear Lots	RLCBMH02A	RLCBMH03A	0.05	0.6	0.75	100 year	0.04	0.00	0.11	10.47	103.71	170.16	0.00	49.67	49.67	0.30%	375	0.013	0.87	20.9	0.40	96.03	52%	514.41	514.35	514.79	514.72	516.42	517.03	1.63	2.31
102	South East Rear Lots	RLCBMH03A	RLCBMH04A	0.08	0.6	0.75	100 year	0.06	0.00	0.17	10.87	101.02	165.80	0.00	76.05	76.05	0.30%	375	0.013	0.87	30.4	0.58	96.03	79%	514.33	514.24	514.70	514.61	517.03	517.24	2.33	2.63
105	South East Rear Lots	RLCBMH04A	RLCBMH05A	0.05	0.6	0.75	100 year	0.04	0.00	0.20	11.45	97.40	159.92	0.00	90.03	90.03	0.30%	375	0.013	0.87	67.4	1.29	96.03	94%	514.22	514.02	514.59	514.39	517.24	516.72	2.65	2.33
112	South East Rear Lots	RLCBMH05A	RLCBMH06A	0.06	0.6	0.75	100 year	0.05	0.00	0.25	12.74	90.38	148.54	0.00	102.21	102.21	0.30%	450	0.013	0.98	20.1	0.34	156.16	65%	513.94	513.88	514.39	514.33	516.72	516.26	1.93	1.93
112A	South East Rear Lots	RLCBMH06A	RLCBMH07A	0.07	0.6	0.75	100 year	0.05	0.00	0.30	13.08	88.72	145.86	0.00	121.65	121.65	0.30%	450	0.013	0.98	20.1	0.34	156.16	78%	513.86	513.80	514.31	514.25	516.26	516.26	1.95	2.01
115	South East Rear Lots	RLCBMH07A	RLCBMH08A	0.02	0.6	0.75	100 year	0.02	0.00	0.32	13.43	87.14	143.29	0.00	125.48	125.48	0.30%	450	0.013	0.98	20.1	0.34	156.16	80%	513.78	513.72	514.23	514.17	516.26	515.86	2.03	1.69
115A	South East Rear Lots	RLCBMH08A	RLCBMH09A	0.07	0.6	0.75	100 year	0.05	0.00	0.37	13.77	85.62	140.83	0.00	143.88	143.88	0.30%	450	0.013	0.98	30.2	0.51	156.16	92%	513.67	513.58	514.12	514.03	515.86	515.80	1.74	1.77
121	South East Rear Lots	RLCBMH09A	RLCBMH10A	0.09	0.6	0.75	100 year	0.07	0.00	0.44	14.28	83.47	137.32	0.00	166.07	166.07	0.30%	525	0.013	1.09	39.6	0.61	235.55	70%	513.50	513.39	514.03	513.91	515.80	515.41	1.77	1.50
121A	South East Rear Lots	RLCBMH10A	RLCBMH11A	0.04	0.6	0.75	100 year	0.03	0.00	0.47	14.89	81.08	133.44	0.00	172.50	172.50	0.30%	525	0.013	1.09	36.5	0.56	235.55	73%	513.37	513.26	513.89	513.78	515.41	514.68	1.52	0.90
121B	South East Rear Lots	RLCBMH11A	STM.MH01A	0.16	0.53	0.66	100 year	0.11	0.00	0.57	15.44	79.01	130.09	0.00	206.50	206.50	0.30%	525	0.013	1.09	17.7	0.27	235.55	88%	513.21	513.15	513.73	513.68	514.68	515.80	0.95	2.12
	South East Rear Lots	STM.MH01A	STM.MH02A	0.00	0	0.00	100 year	0.00	0.00	0.57	15.72	78.06	128.53	0.00	204.03	204.03	0.30%	525	0.013	1.09	67.4	1.03	235.55	87%	513.10	512.90	513.63	513.43	515.80	515.80	2.17	2.38
	South East Rear Lots	STM.MH02A	HW01A	0.00	0	0.00	100 year	0.00	0.00	0.57	16.75	74.66	123.01	0.00	195.27	195.27	0.30%	525	0.013	1.09	16.4	0.25	235.55	83%	512.85	512.80	513.38	513.33	515.80	513.54	2.42	0.22

FIGURES

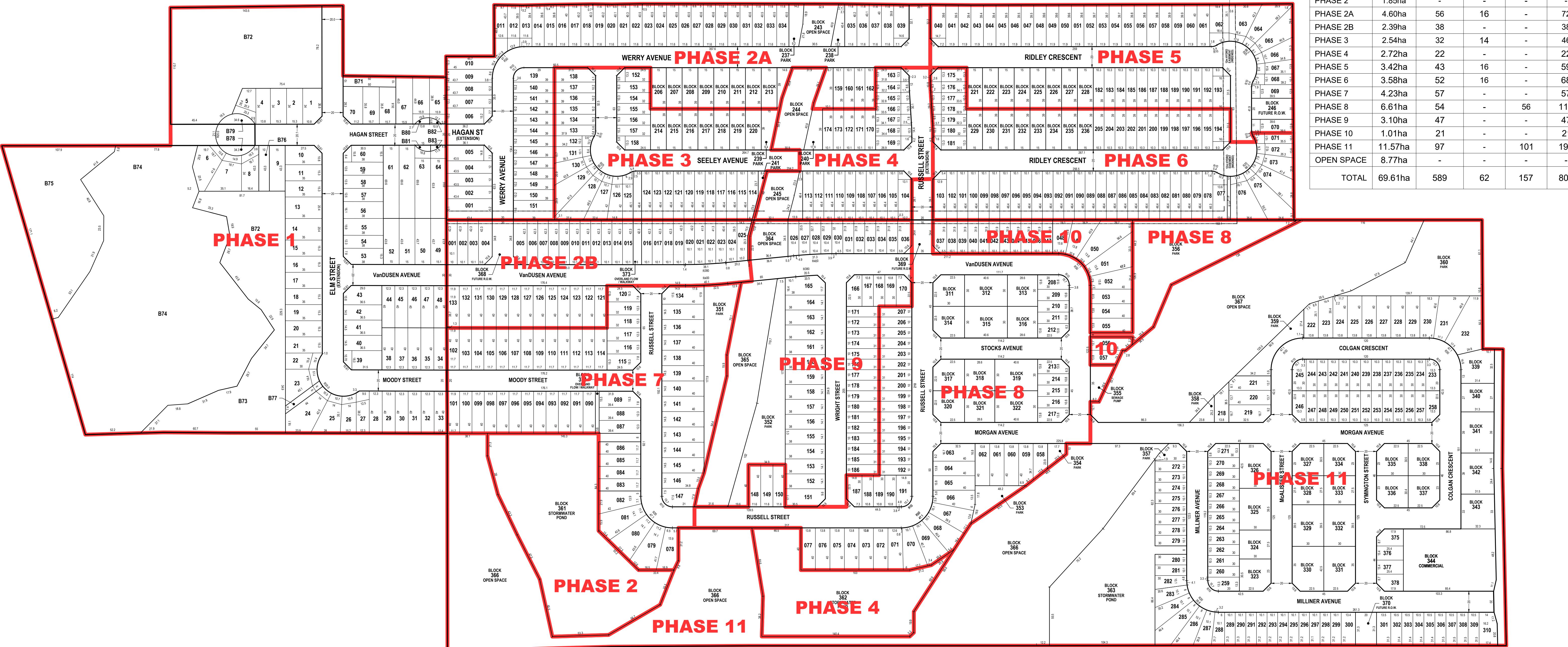
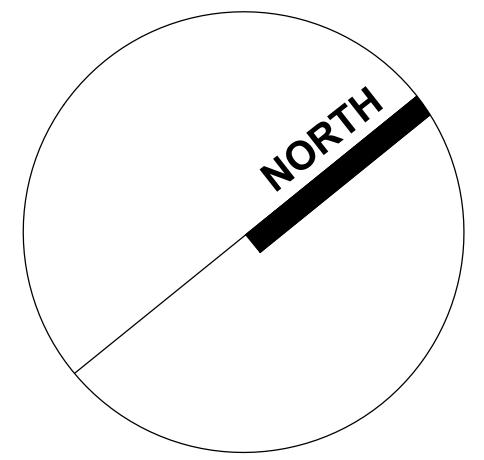
- Figure 1: Site Location Plan
- Figure 2: Flato East Draft Plan
- Figure 3: Edgewood Greens Composite Phasing Plan
- Figure 4: Concept Site Plan
- Figure 5: Pre-Development Drainage Plan
- Drawing C101: General Servicing Plan
- Drawing C102: General Grading Plan
- Drawing C103: Erosion and Sediment Control Plan
- Drawing C104: Construction Staging Plan
- Drawing C109: Sanitary Drainage Plan (Edgewood Greens - Phase 11)
- Drawing C110: Storm Drainage Plan (Edgewood Greens - Phase 11)



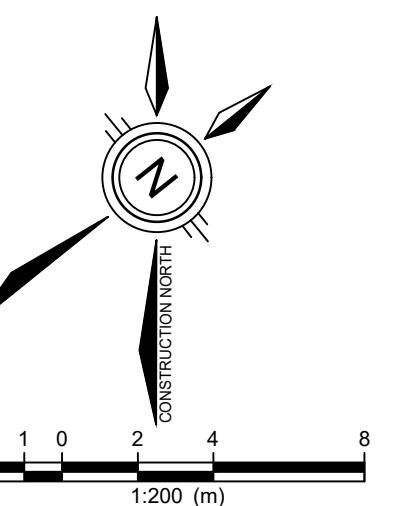
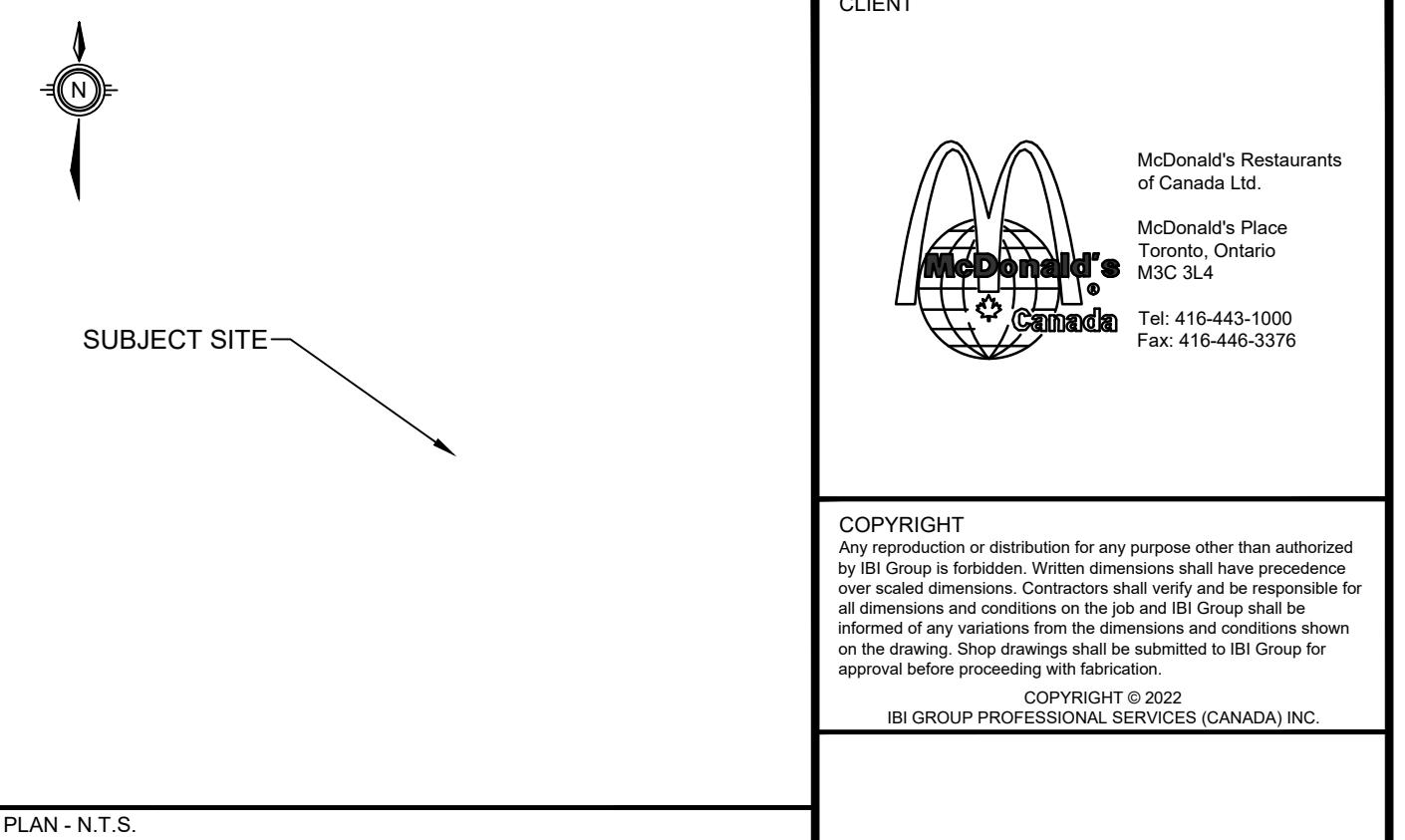
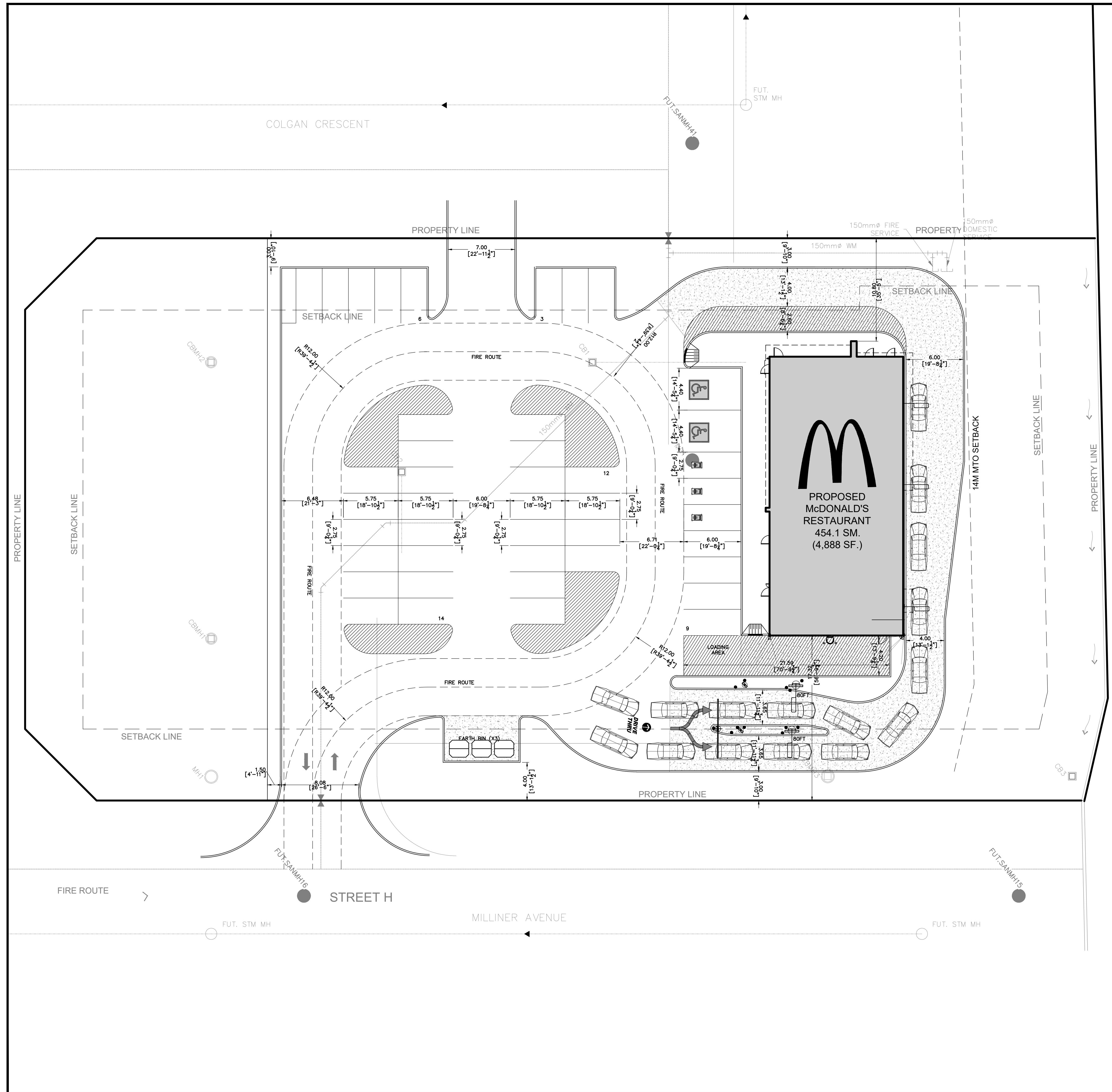
Legend	Project	DUNDALK COMMERCIAL BLOCK TOWNSHIP OF SOUTHGATE				 CROZIER CONSULTING ENGINEERS			
 = SUBJECT DEVELOPMENT	Drawing	SITE LOCATION		Drawn By	T.M.	Design By	A.M.	Project	1060-5384
	Scale	N.T.S.	Date	01/17/2023	Check By	A.M.	Drawing	FIG. 1	



EDGEWOOD GREENS COMPOSITE PHASING PLAN



PHASE	AREA	SINGLES	SEMIS	TOWNS	TOTAL
PHASE 1	13.22ha	70	-	-	70
PHASE 2	1.85ha	-	-	-	-
PHASE 2A	4.60ha	56	16	-	72
PHASE 2B	2.39ha	38	-	-	38
PHASE 3	2.54ha	32	14	-	46
PHASE 4	2.72ha	22	-	-	22
PHASE 5	3.42ha	43	16	-	59
PHASE 6	3.58ha	52	16	-	68
PHASE 7	4.23ha	57	-	-	57
PHASE 8	6.61ha	54	-	56	110
PHASE 9	3.10ha	47	-	-	47
PHASE 10	1.01ha	21	-	-	21
PHASE 11	11.57ha	97	-	101	198
OPEN SPACE	8.77ha	-	-	-	-
TOTAL	69.61ha	589	62	157	808



DATE	BY	DESCRIPTION
DRAWING ISSUE RECORD		

DETAILS OF DEVELOPMENT

DATA	REQUIRED	PROPOSED	
C1-465			
FY (FROM C/L OF ROAD)	32.0 m	>32.0 m	
RY	10.0 m	>10.0 m	
SY (WEST)	3.0 m	10.8 m	
SY (EAST)	3.0 m	17.32 m	
			SEALS

154.4 CM

NOTES

- FEATURES ARE EXISTING UNLESS OTHERWISE NOTED.

DRAWINGS ARE COMPILED FROM INFORMATION SUPPLIED BY OWNER'S AND SHALL BE SITE VERIFIED BY CONTRACTOR AT

COORDINATE AND PROVIDE SERVICING LOCATES TO IBI PRIOR TO CONSTRUCTION START TO CONFIRM THERE ARE NO CONFLICTS WITH PROPOSED.

CONTRACTOR SHALL VERIFY ALL SITE CONDITIONS PERTINENT TO WORK PERFORMED, PRIOR TO STARTING CONSTRUCTION, AND REPORT ANY DISCREPANCIES OR VARIANCES TO PROJECT TEAM.

CONTRACTOR SHALL VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION AND BE RESPONSIBLE FOR SAME.

STRUCTURE SHALL CONFORM TO THE REQUIREMENTS OF LOCAL

McDONALD'S
41288-DUNDALK
HIGHWAY 10, DUNDALK, ON

JECT NO:	140787
WN BY:	SC
O BY:	TW
E:	1:200
E:	2022 10 28
TITLE	CONCRETE PLAN

CONCEPT PLAN

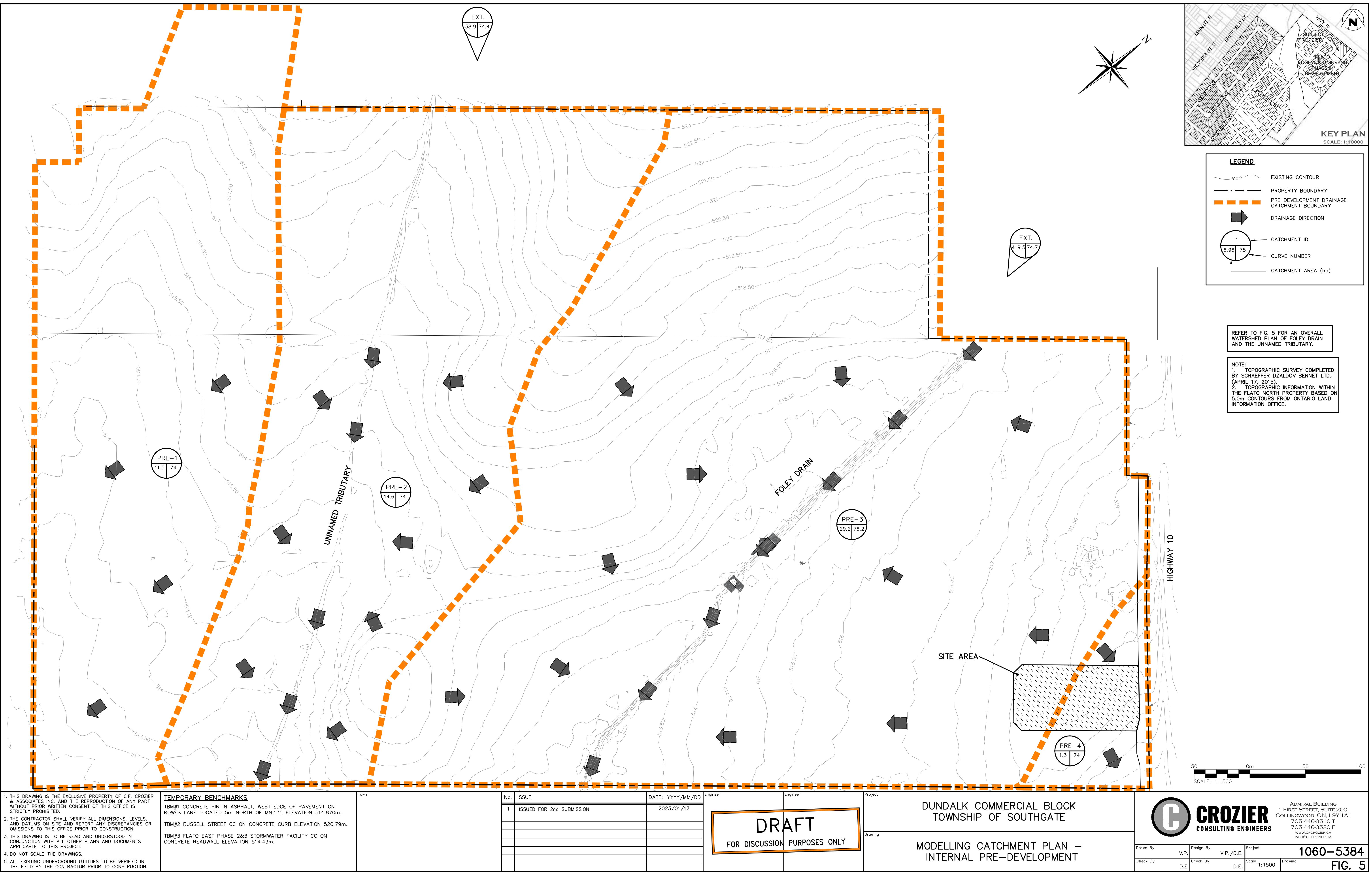
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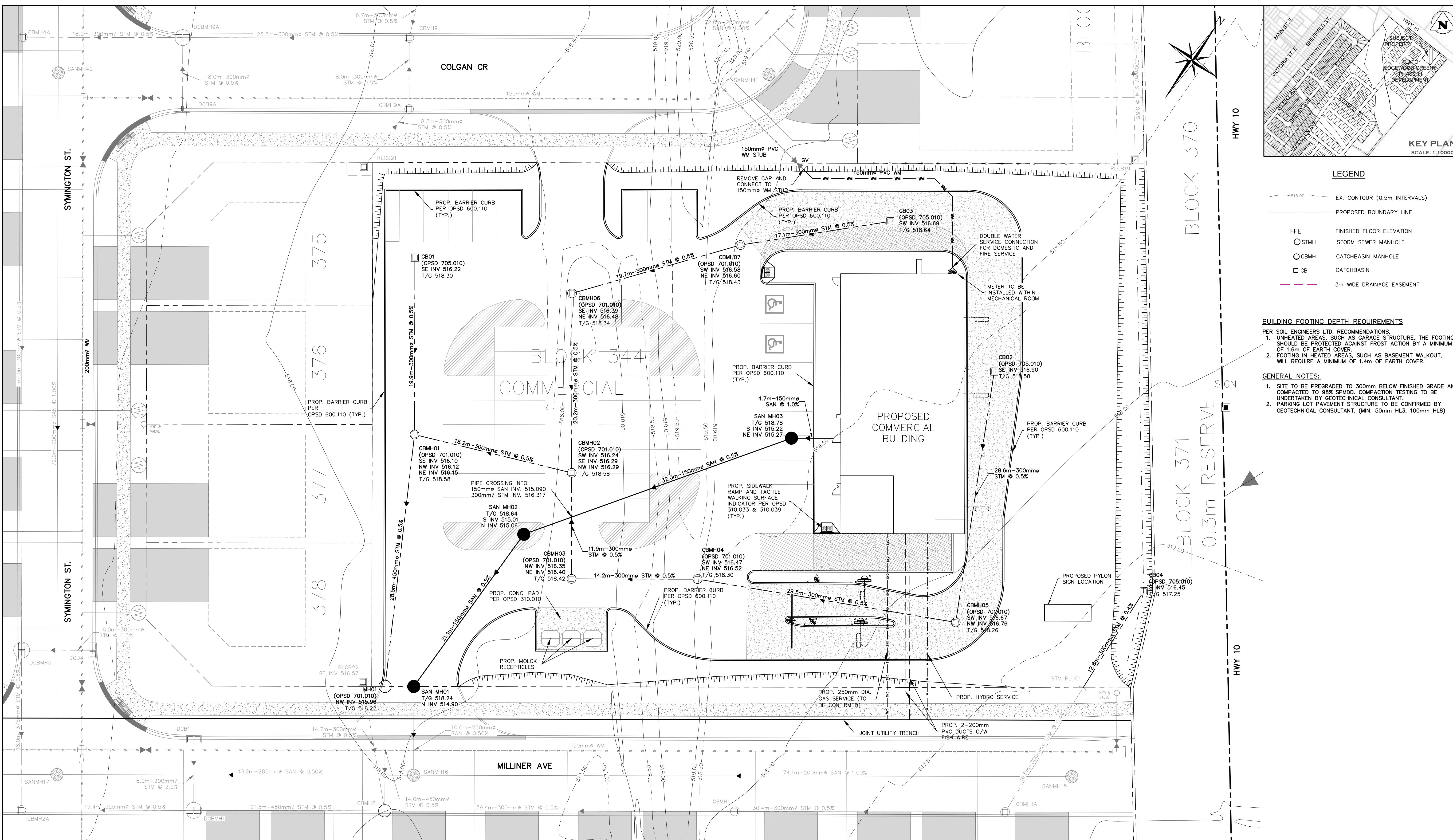
22222222

CP110

14.0

ET 1 OF 1





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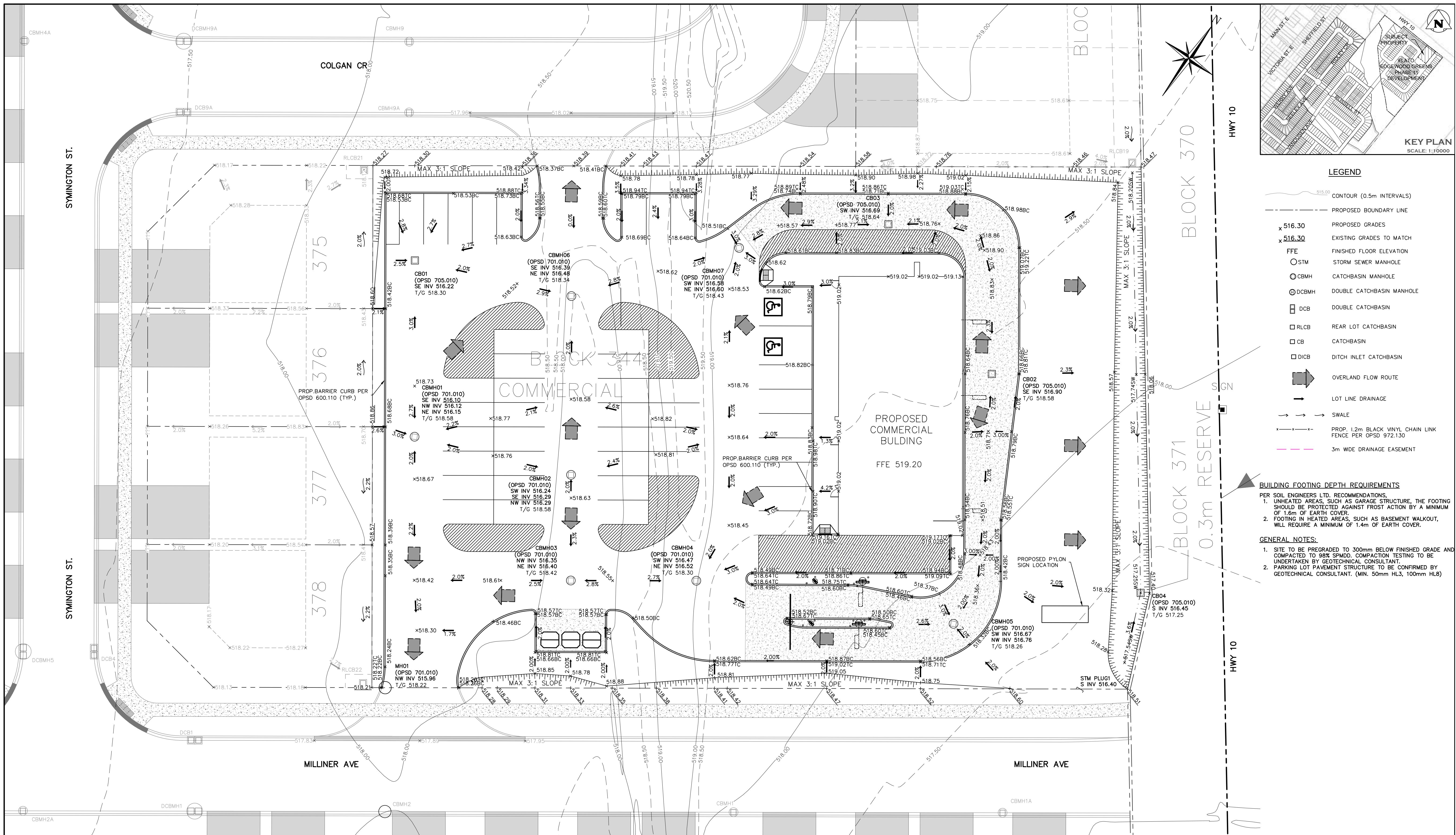
TEMPORARY BENCHMARKS
TBM#1 CONCRETE PIN IN ASPHALT, WEST EDGE OF PAVEMENT ON ROWES LANE LOCATED 5m NORTH OF MN.135 ELEVATION 514.870m.
TBM#2 RUSSELL STREET CC ON CONCRETE CURB ELEVATION 520.79m.
TBM#3 FLATO EAST PHASE 2&3 STORMWATER FACILITY CC ON CONCRETE HEADWALL ELEVATION 514.43m.

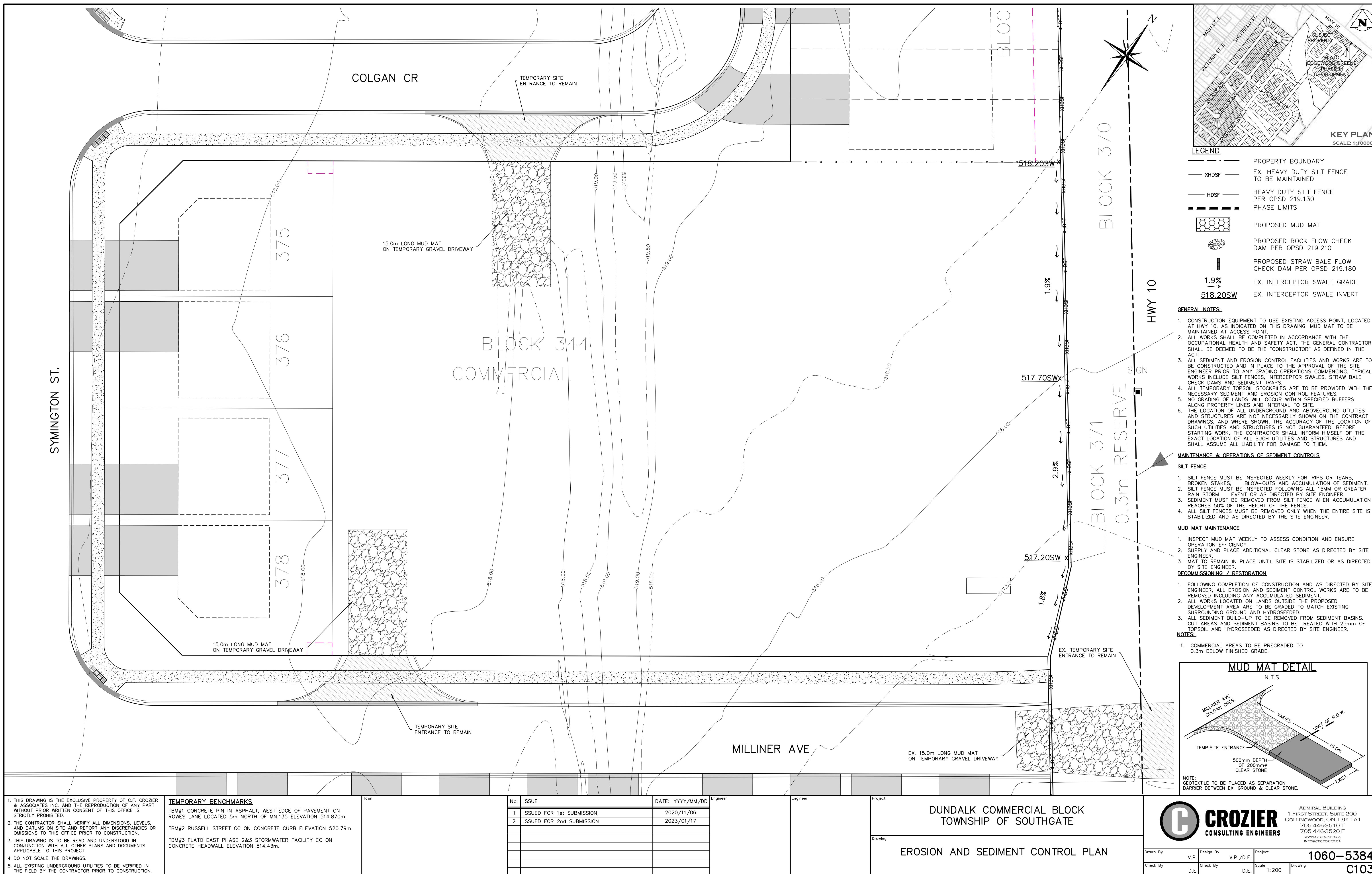
No. ISSUE DATE: YYYY/MM/DD Engineer Engineer Project

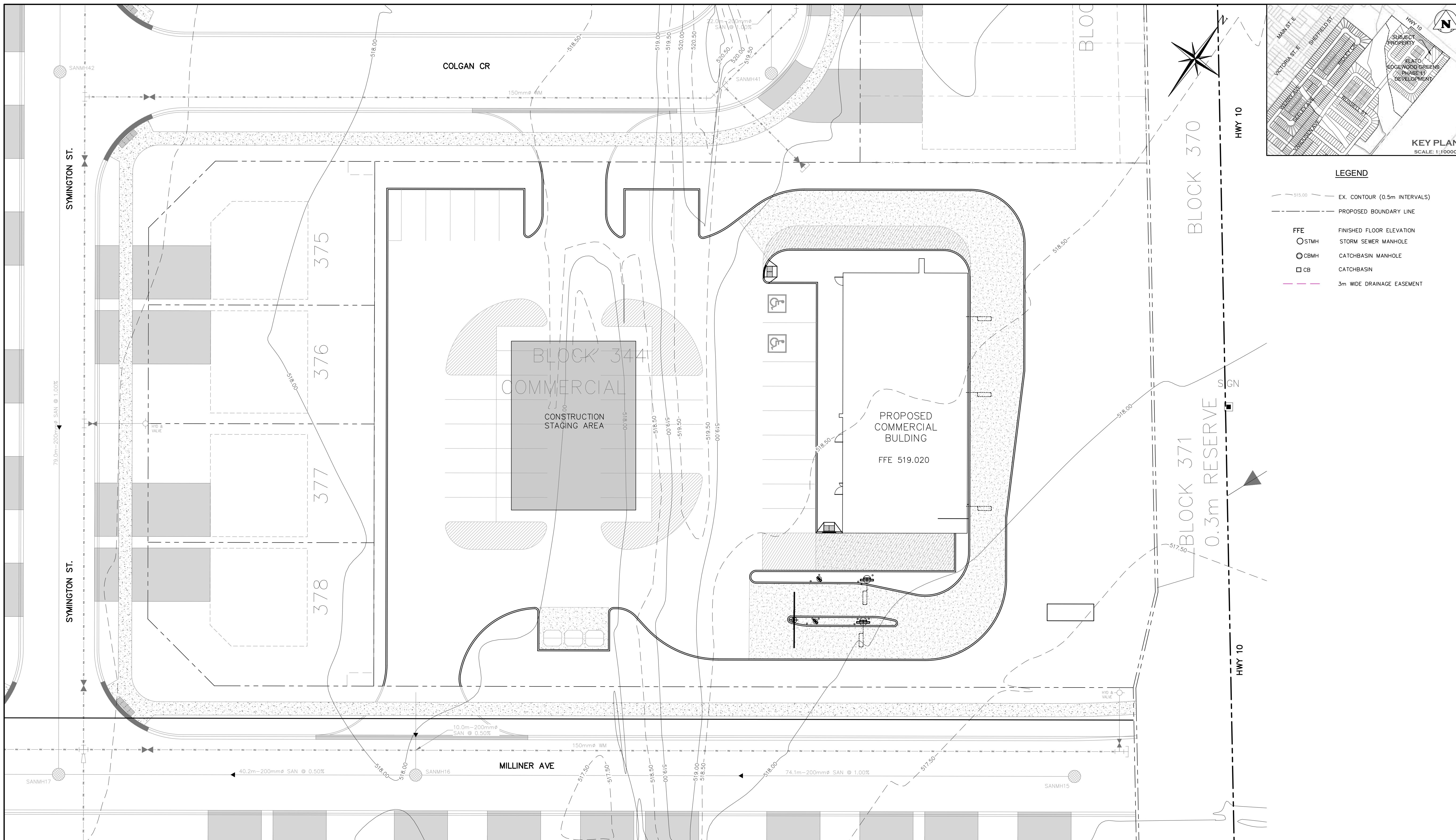
1 ISSUED FOR 1st SUBMISSION 2020/11/06

2 ISSUED FOR 2nd SUBMISSION 2023/01/17

Drawing







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 TBM#3 FLATO EAST PHASE 2&3 STORMWATER FACILITY CC ON CONCRETE HEADWALL ELEVATION 514.43m.

No. ISSUE

DATE: YYYY/MM/DD

Engineer

Engineer

Project

Drawing

DUNDALK COMMERCIAL BLOCK
TOWNSHIP OF SOUTHGATE

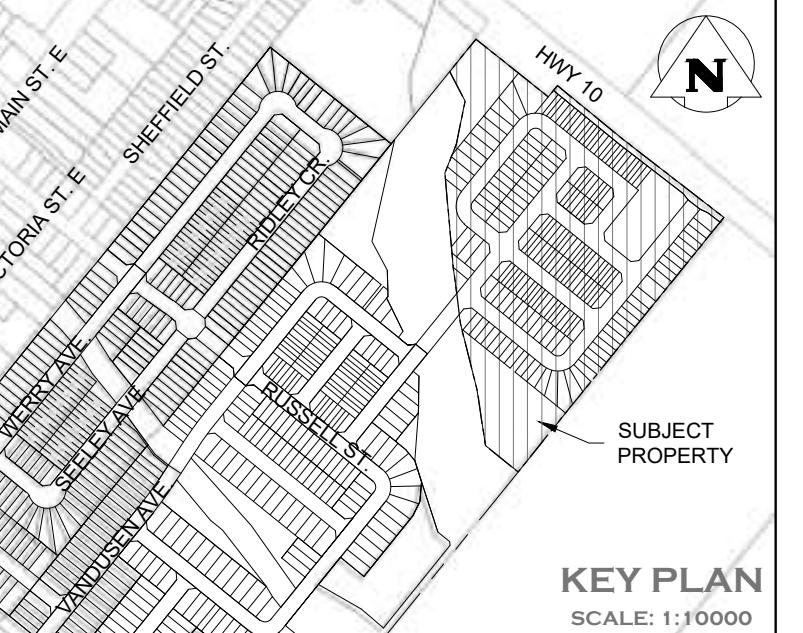
CONSTRUCTION STAGING PLAN



ADIMIR BUILDING
1 FIRST STREET, SUITE 200
COLLINGWOOD, ON, L9Y 1A1
705 446-3510 T
705 446-3520 F
info@crozier.ca
info@crozier.ca

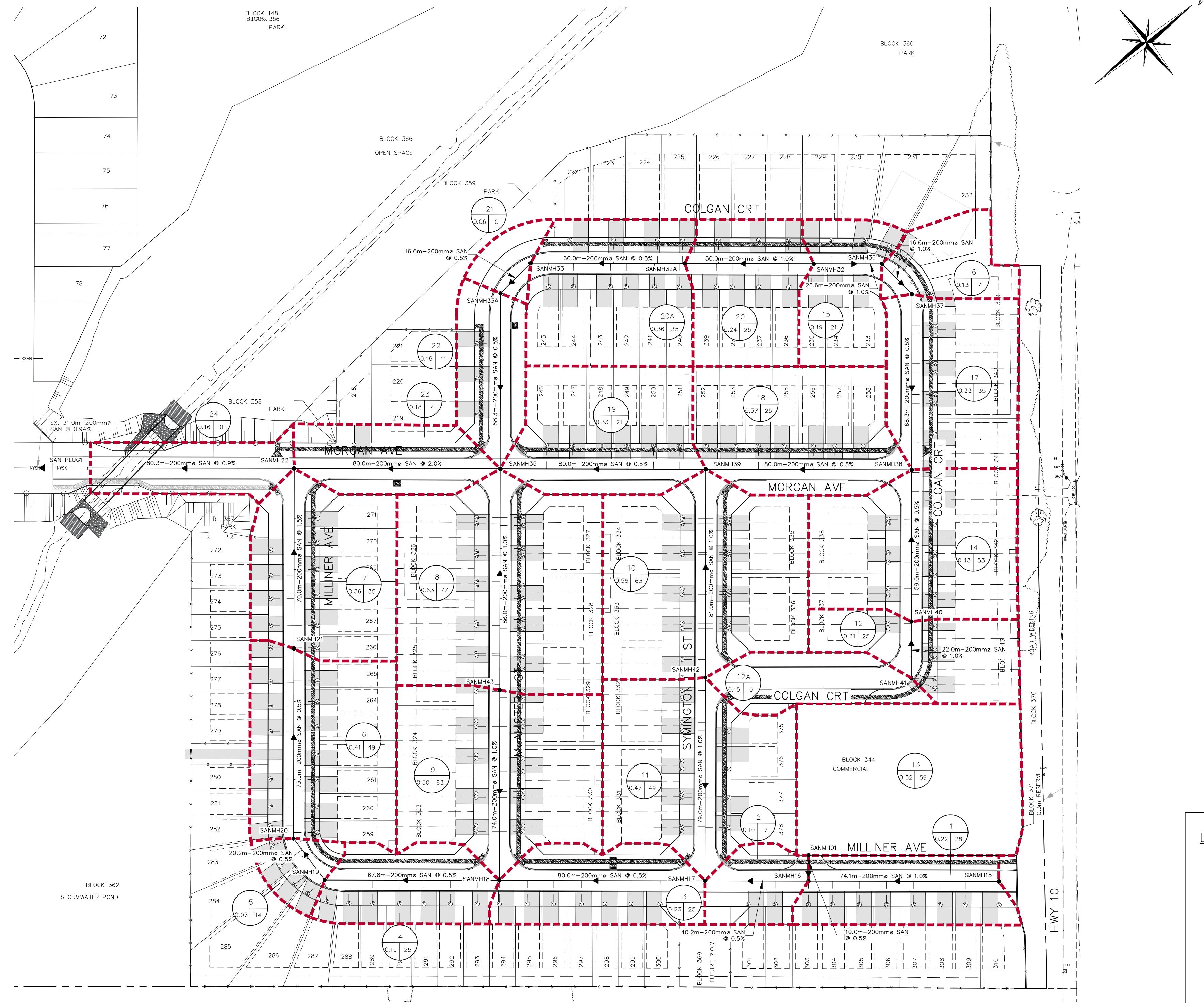
1060-5384
C104

Drawn By V.P. Design By V.P./D.E. Project 1060-5384
Check By D.E. Check By D.E. Scale 1:200 Drawing C104



KEY PLAN

SCALE: 1:10000



LEGEND

- PR. SANITARY SEWER & MANHOLE
- PR. SANITARY CATCHMENT
- SANITARY CATCHMENT AREA ID
- SANITARY CATCHMENT POPULATION (3.5ppu)
- SANITARY CATCHMENT AREA (ha)

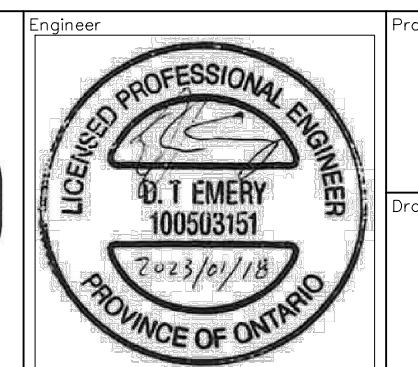
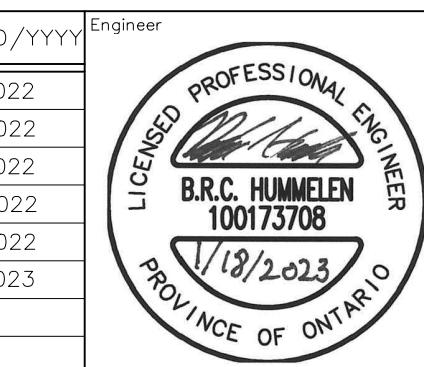
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 TBM#3 FLATO EAST PHASE 2&3 STORMWATER FACILITY CC ON CONCRETE HEADWALL ELEVATION 514.43m.

Town:

No.	ISSUE	DATE: MMM/DD/YYYY	Engineer	Engineer	Project
1	ISSUED FOR 1st SUBMISSION	JAN/10/2022			FLATO EDGEWOOD GREENS
2	ISSUED FOR 2nd SUBMISSION	JUN/24/2022			PHASE 11
3	ISSUED FOR 3rd SUBMISSION	OCT/17/2022			TOWNSHIP OF SOUTHGATE
4	ISSUED FOR TENDER	NOV/07/2022			
5	ISSUED FOR MATERIAL ORDERING	DEC/07/2022			
6	ISSUED FOR 4th SUBMISSION	JAN/18/2023			



Drawing
**FLATO EDGEWOOD GREENS
PHASE 11
TOWNSHIP OF SOUTHGATE**
 SANITARY DRAINAGE PLAN

CROZIER
CONSULTING ENGINEERS
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705 446-3520 F
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INFO@CROZIER.CA
 Drawn By J.K./V.P. Design By V.P./B.H./D.E. Project 1060-5771
 Check By B.H./D.E. Check By B.H./D.E. Scale 1:1000 Drawing C109

