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## **Hydrogeological Assessment**

## Flato Ida

## Flato Ida Dundalk Inc.

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Making Sustainability Happen

### **Revision Record**

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## **Executive Summary**

As part of the Draft Plan of Subdivision and future Site Plan for the proposed Flato Ida residential subdivision, SLR Consulting (Canada) Ltd. (SLR) was retained by Flato Ida Dundalk Inc. (the 'Client') to complete a Hydrogeological Assessment for the subject properties located at 752212, 752226, and 752240 Ida Street in Dundalk, Ontario (the "Site"). These properties are proposed to be developed into a residential subdivision. The purpose of the Hydrogeological Assessment was to examine the hydrogeological characteristics of the Site by reviewing available geological and hydrogeological data to identify any hydrogeological constraints to development, and to provide hydrogeologic guidance when constructing the residential development.

As part of the Hydrogeological Assessment, eight (8) boreholes were advanced by SLR at the 752212 Ida Street property in August 2020 coincident with the Geotechnical Investigation completed by Soil Engineers Ltd. (SEL). Nine (9) additional boreholes were advanced across the remaining land parcels in April 2022. In total, 17 boreholes were advanced across the subject properties through the hydrogeological and geotechnical studies, of which 13 boreholes were completed as monitoring wells, two of which were completed as a nested set. One (1) nested pair of mini-piezometers (consisting of a shallow and deep counterpart) were installed within the wetland area south of the Site across Grey Road 9 (MP1-S/MP1-D) to investigate groundwater-surface water interactions.

The results of the drilling program indicated that the Site is underlain by a discontinuous surficial layer of undifferentiated sediments predominantly comprised of sand to silty sand located at surface overlain by topsoil. At select locations a discontinuous sandy gravel layer was also encountered. Underneath the undifferentiated sediment, the low permeable Elma Till was identified, composed of sandy silt to silty sand material. Based on the Oak Ridges Moraine Groundwater Program, the Till unit is underlain by bedrock. Boreholes advanced across the Site were terminated once the targeted depth of the shallow monitoring wells were reached. As such, bedrock was not encountered during drilling.

Groundwater elevations were measured on a monthly basis at monitors installed at the Site in August 2020 commencing in September 2020. Monitors installed in April 2022 were incorporated into the Groundwater Monitoring Program in May 2022. The most recent monitoring event occurred in March 2024. Water levels fluctuated on a seasonal basis where water levels were relatively shallow in the spring and decreased by approximately 1 m moving into the summer period. Groundwater was interpreted to flow generally in a southwesterly direction along the west portion of the Site and a southeasterly direction along the east portion of the Site. Groundwater elevations were comparable between the shallow and deep nested monitors, indicating that there were negligible hydraulic gradients. Data collected from the nested mini-piezometer location indicated that the wetland feature is primarily precipitation and runoff fed due to generally higher groundwater elevations in the shallower monitor.

It is recognized that portions of the Site are located within a Wellhead protection area (WHPA), an intake protection zone (IPZ), a significant groundwater recharge area SGRA, and a highly vulnerable aquifer (HVA). However, given the thickness of the till aquitard above the bedrock aquifer, there are no anticipated changes to the local water supply due to the proposed development.

There are several wells identified for water supply purposes within a 500 m radius of the site from the MECP Water Well Records (WWR) database. The water supply wells were screened within one of two units: the upper overburden aquifer and the deeper bedrock aquifer.



Wells advanced to depths greater than 20 m are not expected to be impacted by the construction of the subdivision. One water supply well located within a 500 m radius of the Site is screened in a sand gravel deposit located less than 30 mbgs. Should any complaint of well impact from residents be received during the construction of the proposed development, a private water well contingency plan would entail a response within 24 hours to the complaint of depleted or impacted water supply.

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## 1.0 Introduction

SLR Consulting (Canada) Ltd. (SLR) was retained by Flato Ida Dundalk Inc. to conduct a Hydrogeological Assessment in support of a Draft Plan of Subdivision and future Site Plan for the proposed Flato Ida residential subdivision located in Dundalk, Ontario (referred to as the "Site"). The Site includes the properties located at 752212, 752226, and 752240 Ida Street (**Figure 1**). The Site is bounded by Grey Road 9 to the southeast and Ida Street to the northeast. These lands are currently subject to an approved Ministerial Zoning Order (MZO).

#### 1.1 Study Objectives

The objective of the Hydrogeological Assessment is to characterize the hydrogeological conditions across the Site, identify any hydrogeological constraints to development and potential impacts of development on natural heritage features, and provide guidance on how to mitigate these impacts. This is completed through a review of relevant geologic and hydrogeologic information available through public records for the area or collected through borehole drilling and groundwater monitoring and sampling efforts. This report has been prepared for submission to the Township of Southgate, Saugeen Valley Conservation Authority (SVCA), and Grand River Conservation Authority (GRCA) to support the Draft Plan of Subdivision and future Site Plan Approval for the proposed development.

The specific objectives are summarized below:

- Document the geology, hydrostratigraphy, groundwater flow, and groundwater quality across the Study Area.
- Evaluate potential impacts with respect to Source Protection Plans.
- Assess overall potential impacts of the proposed development on the groundwater flow system.

#### 1.2 Report Organization

This Hydrogeology Assessment report has been organized into eight sections following this introduction. Section 2 provides an overview of background information related to the development, previous investigations and regional geology and hydrogeology. Section 3 provides the field methodologies utilized during the assessment. Section 4 presents a review of the Site geologic and hydrogeologic conditions. Section 5 provides an assessment of the potential impacts of development on shallow groundwater features, potable wells and surface water features. Section 6 presents the conclusions and recommendations. Section 7 provides a closing statement and Section 8 presents the report references.

All Figures referenced throughout the report are presented within the text. Appendices A through E present the: Proposed Development Plan; Borehole Logs; Groundwater Data; AQTESOLV Analyses; and MECP Water Well Records, respectively.

## 2.0 Background

#### 2.1 Proposed Development

The Site is irregular in shape and measures approximately 35.9 ha in size. The proposed development area measures approximately 18.7 ha, with the remaining 17.2 ha considered non-developable area. It is understood that the proposed development will contain single detached lots, apartment complex, pumping station, stormwater management (SWM) pond, parks, and areas of environmental protection. A copy of the proposed development plan is provided in **Appendix A**.

#### 2.2 Site Description

The proposed Flato Ida residential subdivision lies on lands legally described as Parts of Lots 228, 229 and 230, Range 3 West of the Toronto and Sydenham Road Geographic Township of Proton, Township of Southgate, County of Grey. The Site is bounded by Grey Road 9 to the southeast and Ida Street to the northeast (**Figure 2**). Agricultural and vacant land is present to the northwest, with a forested area and associated wetland to the southwest. The Site, as well as the surrounding area, is used primarily for agricultural purposes, with scattered rural residences.

#### 2.3 Regional setting

#### 2.3.1 Topography and Drainage

The Site is gently undulating with a gentle decrease in ground surface elevation from north to south. A topographic high of 519 metres above sea level (masl) is located near the north end of the Site, with a topographic low of 509 masl at the southwestern boundary (**Figure 3**).

The Site is located on a drainage divide between the Saugeen River Watershed (SRW) and Upper Grand River Watershed (GRW), which are governed by the SVCA and GRCA, respectively.

A Willow Mineral Thicket Swamp is situated in the southern portion of the site abutting the property boundary to the south and east, and agricultural lands and cultural meadow to the north and west, respectively (**Figure 3**). Additionally, a large Poplar-Conifer Mineral Mixed Swamp wetland community is located at the south end of the site and extends to the west beyond the property boundary. An evaluation of the wetlands will be completed as part of the Environmental Impact Study (EIS), to be provided under separate cover (SLR, 2024).

In addition, a tributary to the Grand River headwater drainage feature (HDF) and its associated floodplain is located within the GRW (**Figure 3**). This drainage feature includes a pond at the headwaters, suggesting groundwater dependence. The drainage feature drains towards to the south towards a wetland south of Grey Road 9. Surface water was present within the drainage feature during spring monitoring and water levels near or above ground surface in wells adjacent to the feature (as discussed below) but dry during summer months.

#### 2.3.2 Physiography

The Study Area lies within the Dundalk Till Plain physiographic region of southern Ontario (Chapman and Putnam, 1984).



The Dundalk Till Plain is a gently undulating, partially drumlinized and fluted surface, where the long axis of the drumlins are oriented in a southeastward direction. The Dundalk Till Plain supports extensive wetland complexes due to the presence of poorly drained depressions.

#### 2.3.3 Regional Hydrostratigraphy

Surficial geology in the Dundalk area mainly consists of drumlinized till plains (Chapman and Putnam, 1984) comprised of the Elma Till (stony sandy silt to silt) and Catfish Creek Till (clayey silt and gravel).

There are isolated deposits of glaciolacustrine, glaciofluvial ice-contact and glaciofluvial outwash materials at surface and interbedded within the till plain. These sand and gravel deposits forms the Dundalk Aquifer (Saugeen Valley Source Protection Area, 2015). The extent and thickness of the Dundalk Aquifer is unknown, due to a lack of reliable well records for the area. It is noted that static water levels within the Dundalk Aquifer is close to ground surface.

The overburden material is underlain by bedrock aquifer units comprised of the Guelph, Eramosa, Goat Island and Gasport Formations (Golder, 2018).

#### 2.3.4 Source Protection

Source Protection Plans (SPPs) have been implemented throughout the region to protect drinking water resources, as mandated by the *Ontario Clean Water Act*, 2006. The susceptibility of an aquifer to contamination is evaluated to identify the most vulnerable areas surrounding a drinking water source. There are four (4) types of vulnerable areas as defined by the *Ontario Clean Water Act*, 2006:

- Highly vulnerable aquifer (HVA): aquifers in which an external source is likely to have a significant adverse effect, this includes the land above the aquifer;
- Significant groundwater recharge area (SGRA): an area in which it is necessary to regulate or monitor drinking water threats, that could affect the recharge of an aquifer;
- Surface water intake protection zone (IPZ): an area related to a surface water intake area in which it is necessary to regulate or monitor drinking water threats; and
- Wellhead protection area (WHPA): an area related to a wellhead, within which it is necessary to regulate or monitor drinking water threats.

The Site is within both the Saugeen River Source Protection Plan and the Grand River Source Protection Plan. The Grand River Source Protection Plan has identified the eastern portion of the Site to be within an IPZ and SGRA (**Figure 4**). In addition, the Saugeen River Source Protection Plan has identified the western portion of the Site to be within a SGRA and highly vulnerable aquifer (**Figure 4**). The eastern portion of the Site is also located within a WHPA-D (**Figure 5**) representing a 25-year time-of-travel zone, with the nearest municipal well located approximately 550 m northeast of the Site boundary.

Groundwater and surface water resources within an IPZ, SGRA, HVA, and WHPA are relatively sensitive to chemical or pathogen contamination and / or changes in groundwater recharge. Although precautionary measures to protect groundwater and surface water must be applied on all projects, additional protection measures and related documentation may be required where study areas fall within these zones. These include maintenance of the site-wide water balance and limitations on the presence of potential contamination sources such as gas stations and dry cleaner facilities. Based on the current development plan, the Site development does not include any commercial facilities.



It is important to note that delineation of the vulnerable areas is based on regional mapping and does not consider site-specific conditions (i.e., type and thickness of the overlying material). The results of the drilling program indicates that the subsurface soils across the Site consist of a thin (1-2 m thick) sand to silty sand unit underlain by silty sand to sandy silt till.

Additionally, mapping indicates surficial geology consisting predominantly of sandy silt to silty sand till. The till unit was determined to have low hydraulic conductivity and therefore, the potential to impact deeper aquifers is limited.

A site-specific water balance has been completed by Crozier & Associates Consulting Engineers ("Crozier") to document pre-development recharge rates, and to look for opportunities to promote the recharge of clean water to meet or exceed pre-development recharge rates. The site-specific water balance is presented under separate cover.

## 3.0 Methodology

#### 3.1 Installation of Groundwater Monitors

Eight (8) boreholes were advanced at select locations across the 752212 Ida Street property in August 2020 coincident with the Geotechnical Investigation completed by Soil Engineers Ltd. (SEL). Nine (9) additional boreholes were advanced as part of additional investigations by SLR in April 2022 across the remaining land parcels after their acquisition by Flato Ida Dundalk Inc. The boreholes were drilled using a track-mounted drill rig with 0.20 m outer diameter hollow stem auger. A record of geological and hydrogeological conditions was logged during drilling using a split spoon sampler at approximately 0.76 m intervals down to the targeted depth of the monitoring well. At each borehole location, the soil stratigraphy and classification, moisture content, colour, appearance, soil structure (presence of laminations, heterogeneity, soil weathering, etc.), and odour was noted in general accordance with the Unified Soil Classification System.

Select borehole locations (**Figure 2**) were completed as monitoring wells, whereby nested monitoring wells consisting of a shallow and deep counterpart were installed at MW-7 and MW22-405. All monitoring wells were constructed with a 50-millimetre (mm) diameter polyvinyl chloride (PVC) well pipe. In general, the monitoring wells were constructed with No. 10 slotted PVC screen approximately 1.5 m long. Monitor ESA-1 was installed near a suspected aboveground storage tank (AST) and underground storage tank (UST) as part of a Phase 2 Environmental Site Assessment completed coincident with the additional drilling program in 2022 (SLR, 2022). A longer screen (3.0 m long) was installed at this location to allow for an assessment of potential petroleum impacts. The results of the Phase 2 Environmental Site Assessment are provided under separate cover and not discussed herein.

A sand pack was placed around and slightly above the well screen with the remaining upper portion of the borehole was sealed with bentonite. A steel monument casing was installed over the well at each monitoring location. Upon completion of the monitoring wells, the monitors were tagged and registered with the MECP as required by Ontario Regulation (O. Reg.) 903, as amended. Details of the monitoring well construction are summarized in **Table 3-1**. The locations of the monitoring wells are depicted in (**Figure 2**), and borehole logs are provided in **Appendix B**.

One (1) nested pair of mini-piezometers (consisting of a shallow and deep counterpart) were installed within the wetland area south of the Site across Grey Road 9 (MP1-S/MP1-D). The mini-piezometers were installed to assess groundwater-surface water interactions within the wetland. The mini-piezometers were constructed with a 19 mm diameter steel pipe threaded onto an approximately 0.33 m long screened drive point piezometer tip, and were installed to the targeted depth through direct push. A pilot hole was not advanced prior to the installation; as such, the screened material at the mini-piezometers is unknown. The location of the mini-piezometers are shown on (**Figure 2**).

Table	3-1:	Monitoring	Well	Details
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Monitor	Date of Installation	Ground Surface Elevation (masl)	Top of Pipe Elevation (masl)	Screen Interval (masl)	Screened Material
ESA-1	13-Apr-2022	514.2	515.2	512.6 - 509.6	Silty SAND TILL
MW22-401	13-Apr-2022	518.6	519.5	514.0 - 512.5	Silty SAND TILL
MW22-402	11-Apr-2022	516.8	517.7	512.3 - 510.7	Silty SAND TILL
MW22-403	11-Apr-2022	514.3	515.2	509.7 - 508.2	Sandy SILT TILL
MW22-404	13-Apr-2022	514.2	515.0	509.6 - 508.1	Silty SAND TILL
MW22-405-S	12-Apr-2022	512.1	513.1	507.5 - 506.0	Silty SAND TILL
MW22-405-D	12-Apr-2022	512.1	513.1	503.0 - 501.4	Silty SAND TILL
MW22-406	18-Apr-2022	511.5	512.3	507.2 - 505.7	Silty SAND TILL, SANDY GRAVEL
MW22-407	18-Apr-2022	509.5	510.5	505.0 - 503.5	Sandy SILT TILL
MW22-408	18-Apr-2022	509.3	510.3	504.7 - 503.2	Silty SAND with GRAVEL
MW-2	26-Aug-2020	513.5	514.3	510.6 - 509.1	Silty SAND TILL, SAND
MW-6	24-Aug-2020	514.8	515.5	511.9 - 510.4	Silty SAND TILL, SAND
MW-7-S	25-Aug-2020	512.1	512.7	510.7 - 509.2	Silty SAND TILL, SAND
MW-7-D	24-Aug-2020	512.1	512.7	507.5 - 505.9	Silty SAND TILL
MW-8	26-Aug-2020	513.6	514.5	511.7 – 510.1	Silty SAND TILL
MP-1-S	16-Oct-2020	510.6	511.4	-	-
MP-1-D	16-Oct-2020	510.5	511.9	-	-

### 3.2 Monitoring Well Development

Following installation, the monitoring wells were developed using dedicated tubing fitted with Waterra inertia foot valves.

The monitoring wells were developed to remove any soil fines that may have infiltrated into the monitoring well and its surrounding sand pack during the installation process, and to improve the hydraulic connection between the well and geologic materials. Due to slow recovery, each well was purged dry and allowed to recover. Water was subsequently removed from the monitoring well until discontinuous flow was produced for a second time.

### 3.3 Water Level Monitoring

Groundwater levels were manually collected on an approximately quarterly basis in each accessible monitor using a water level meter to collect baseline data prior to development. Groundwater monitoring commenced in September 2020 within the 752212 Ida Street land parcel, and the remaining monitors were incorporated into the program in May 2022. The most recent groundwater monitoring event occurred on March 7, 2024.

The surface water level and groundwater elevation were measured at the mini-piezometer location to assess groundwater-surface water interactions within the wetland area.

To support a more comprehensive understanding of the Site, select monitoring wells and minipiezometers were instrumented with automated dataloggers to obtain continuous groundwater level readings at 12-hour intervals. A barologger was also deployed coincident with the dataloggers to measure changes in atmospheric pressure. Continuous water level measurements provide additional insight into the groundwater regime, particularly in response to precipitation events, as well as high-water level conditions. The dataloggers are downloaded every four (4) months while completing manual water level measurements on-Site. The datalogger was removed from the mini-piezometers in November 2021, and was subsequently monitored by manual measurements during the quarterly water level events. Dataloggers were removed from groundwater wells on November 1, 2023.

#### 3.4 In-Situ Hydraulic Conductivity and Analysis

In-situ hydraulic conductivity tests were completed in select monitoring wells to establish the permeability (hydraulic conductivity) of the formation in which the wells are screened. Hydraulic conductivity is a parameter that describes the ability of soil to allow water to move through it. The lower the hydraulic conductivity, the less water will be able to move through. Aquifers, such as sandy or gravelly soils, typically have a hydraulic conductivity of 10<sup>-6</sup> metres per second (m/s) or greater, whereas aquitards (clay or dense silt) have a hydraulic conductivity of 10<sup>-8</sup> m/s or less.

The testing involved the slug test method, whereby a slug of known volume was removed (rising head test) from each well. The water levels were recorded during the addition, removal, and recovery stages of the slug test using a Diver datalogger temporarily installed in the monitor. The in-situ hydraulic conductivity test was completed once the water level recovered to 90% of static conditions. The slug tests were analyzed in AQTESOLV using the Bouwer-Rice method (1976) for unconfined aquifers.

#### 3.5 Gas Monitoring

Gas probes were installed at four select monitors (ESA-1, MW-2, MW-6, MW-7-S) on March 1, 2024, to support the ongoing D4 Investigation for the Site (submitted under separate cover). At the time of installation, groundwater levels were above the well screen and gas monitoring was not feasible.

The potential for gas migration is greatest under frozen ground conditions, when combustible gases, if present, will tend to preferentially migrate laterally through the soils rather than vent through the overlying fill or cover material. Therefore, to assess for the presence and temporal variability of soil gas concentrations, it is recommended that soil gas monitoring occurs at minimum, during periods of low water table (Summer 2024) and frozen conditions (Winter 2024/2025).

## 4.0 Site Geology and Hydrogeology

#### 4.1 Geology and Hydrostratigraphy

#### 4.1.1 Surficial Geology

Based on a review of the Ontario Geological Survey mapping (OGS, 2010), surficial geology of the Site is primarily Elma Till, which is characterized as a stone-poor sandy silt to silty sand till. Localized glaciofluvial sand deposits are found along the western and southern property boundary within the wetland area (**Figure 6**).

Surficial geology of the Site was also characterized by advancing boreholes at select locations across the property. Borehole logs are provided in **Appendix B**. Geological cross-sections of the Site, as indicated in (**Figure 7**), are presented in (**Figure 8** and **Figure 9**).

Based on the results of the drilling program, a relatively thin (1–2 m thick) sand to silty sand unit was located at surface overlain by topsoil. At select locations (MW22-405, MW22-406, MW22-408), a discontinuous sandy gravel layer was encountered between depths of 1.5 mbgs to 6.8 mbgs, or about 510.6 masl to 502.5 masl.

A till unit was found underlying the sand to silty sand unit. The till unit is composed of sandy silt to silty sand material and was located at approximately 516.3 masl (2.3 mbgs) (MW22-401) to 506.2 masl (5.3 mbgs) (MW22-406). Interbedded within the till unit are discontinuous sand to sandy gravel lenses. The upper 3 to 5 m of the till unit is weathered, and shows root structures, fractures, and oxidized soils. This more permeable weathered soil hosts the water table, primarily due to poor drainage to depth. The glacial till is estimated to be approximately 35 m thick underneath the Site. The glacial till material serves as an aquitard protecting the underlying bedrock aquifer due to its low permeability and substantial thickness.

#### 4.1.2 Bedrock Geology

Boreholes advanced across the Site were terminated once the targeted depth of the monitoring wells were reached. As such, bedrock was not encountered during drilling. However, a review of the MECP WWR database (**Figure 11**) indicates that the bedrock in the area generally lies between 26 mbgs (MECP well ID 2513888) to 74 mbgs (MECP well ID 2509298). There was also one well record (MECP well ID 2500875) that encountered bedrock at 112.5 mbgs. The bedrock consists mostly of dolostone/limestone. It is noted that one well (MECP well ID 2502018), located approximately 500 m northwest of the Site, encountered shale at 34 mbgs.

Source Protection documents from the GRCA indicates that the bedrock is composed of 88 m of both the Guelph Formation and the Gasport Formation (Lake Erie Region Source Protection Committee, 2021). The Guelph Formation consists of porous, fine to medium crystalline, medium to massive irregularly bedded dolostone, while the underlying Gasport Formation consists of thick- to massive-bedded, fine to coarse-grained dolostone and dolomitic limestone (Armstrong, 2010).

## 4.2 Groundwater Monitoring

#### 4.2.1 Groundwater Levels

Groundwater level measurements were recorded at monitors MW-2, MW-6, MW-7-S/D, MW-8 and MP1-S/D commencing in September 2020 with the most recent monitoring event occurring in March 2024. Monitors ESA-1, MW22-401, MW22-402, MW22-403, MW22-404, MW22-405-S/D, MW22-406, MW22-407, and MW22-408 were incorporated into the Groundwater Monitoring Program in May 2022. Monitors MP1-S/D, MW-6, MW-7-S/D, MW22-405-S/D, MW22-406, and MW22-408 were instrumented with dataloggers to collect continuous water level measurements at 12-hour intervals. Groundwater elevations measured within the monitoring wells and mini-piezometers are provided in **Table C-1** to **C-2**, **Appendix C**, and hydrographs are provided in **Appendix C**.

Groundwater elevations across the Site ranged between -0.7 mbgs to 3.9 mbgs, or 507.2 masl to 517.7 masl, and subtly followed surface topography, where the highest and lowest water levels were consistently observed at MW22-401 (northern portion of the Site) and MW22-407 (southern portion of the Site), respectively.

During the groundwater monitoring period, water levels were observed to display seasonality. Groundwater elevations were highest in the spring season with levels at or near ground surface, and slowly declined over the course of the summer. Groundwater levels can be seen rising following the fall season and appear relatively stable until the following spring.

Noted periods of drawdown occurred in June 2021 and August 2021 in MW-7 S/D and MW-6 (**Appendix C**). Additionally, MW-6 exhibited a drawdown in February 2021 and February 2022, which was not seen in MW-7. A general declining trend in water levels was observed in all monitoring wells with data loggers between May and September 2022. Groundwater levels exhibit increasing trends until the following December. A decrease is again observed in summer 2023 with subsequent increasing trends in fall up to logger removal from the wells in November 2023.

Groundwater monitoring results within the wetlands on the southwestern portion of the Site suggest that high water levels are present during the spring, with the low permeable soils providing limited infiltration. During the warmer summer months, the water table drops and no groundwater input is provided to the wetland. However, within the larger wetland/woodland swamp, the soils consist of a more permeable sands and gravels pocket, which collects drainage from the Site (both surface water and groundwater). But due to the limited extent of the surficial sand and gravel zone (**Figure 6**), the water has no outlet to drain, and results in saturated conditions throughout the year.

#### 4.2.2 Horizontal Groundwater Flow

The interpreted groundwater contours for spring 2023, representing a generally high-water table position, are presented in (**Figure 10**). Water levels during spring conditions are of particular interest as it typically represents the highest groundwater elevations and will therefore inform the engineering design of residential development. The interpreted groundwater flow direction is primarily in southwesterly direction along the west portion of the Site and a southeasterly direction along the east portion of the Site. It is noted that there is a watershed drainage divide that runs through the centre of the Site in a north-south direction. The horizontal component of groundwater flow during the spring season travels in the weathered upper till, surficial sand, silty sand, and sand with gravel.

#### 4.2.3 Vertical Groundwater Flow

Vertical hydraulic gradients were calculated between the shallow and deep monitors at the nested monitoring well locations to assess groundwater discharge/recharge conditions. Vertical hydraulic gradients were also calculated at the mini-piezometer location to assess groundwater-surface water interactions within the wetland located east of the Site. The vertical hydraulic gradients are provided in **Table C-3**, **Appendix C**.

Groundwater elevations were comparable (**Figure C-1, Appendix C**) between the shallow and deep monitor at nested monitoring wells MW22-405 and MW-7, indicating that there were negligible (i.e., 0.00 to 0.03 m/m) hydraulic gradients. The shallow and deep monitors at each nested monitoring well locations were screened within the silty sand to sandy silt till unit, suggesting that there was consistently negligible vertical movement within the till.

At mini-piezometer location MP1, groundwater elevations were generally higher in the shallow monitor compared to its deeper counterpart. This indicates that the wetland feature is primarily precipitation and runoff fed. During the spring season following snowmelt and during large precipitation events, there are sporadic groundwater contributions to the wetland.

#### 4.3 Hydraulic Conductivity

In-situ hydraulic conductivity tests were completed at two (2) groundwater monitoring wells at the Site. The results of the hydraulic conductivity tests are provided in **Table 4-1**, and the AQTESOLV analysis are provided in **Appendix D**.

Monitor	Hydraulic Conductivity (m/s)	Screened Strata	
MW22-405-S	8.2 x 10 <sup>-8</sup>	Silty SAND TILL	
MW22-405-D	1.8 x 10 <sup>-8</sup>	Silty SAND TILL	

#### Table 4-1: Hydraulic Conductivity

The geometric mean hydraulic conductivity for the tested monitoring wells is  $3.8 \times 10^{-8}$  m/s, with a measured range of  $1.8 \times 10^{-8}$  to  $8.2 \times 10^{-8}$  m/s. This corresponds to the upper weathered portion of the glacial till. A deeper monitor, located within a nearby development area located approximately 800 m north of the Site, was screened within the unweathered glacial till aquitard and was found to have a hydraulic conductivity 30 times lower than the upper material at 7.6 x  $10^{-10}$  m/s (SLR, 2023). The results are consistent with those reported by Freeze and Cherry (1979) for similar soils.

#### 4.4 MECP Water Well Record Database

Well records from the MECP WWR database were reviewed<sup>1</sup> to assess the stratigraphy and water use of wells located within a 500 m radius of the Site. The locations of the wells are shown in (**Figure 10**), and a summary is provided in **Appendix E**. Copies of the well records are provided in **Appendix E**.

<sup>&</sup>lt;sup>1</sup> The MECP WWR database was reviewed in April 2024.

Forty-three (43) MECP records were identified for wells listed to be within 500 m of the property. Twenty-three (23) of those records were for wells for water supply purposes, sixteen (16) were observation/monitoring wells or test holes, and four (4) were noted to be abandoned. The water supply wells were screened within one of two units: the upper overburden aquifer and the deeper bedrock aquifer.

The bedrock aquifer is composed of both the Guelph Dolostone Formation and the underlying Gasport Dolostone Formation. Based on available MECP well records, the bedrock surface generally lies between 26 mbgs (MECP well ID 2513888) to 74 mbgs (MECP well ID 2509298). The upper bedrock is inferred to be of low permeability, and the municipal production zone lies in the middle of the sequence. Municipal Wells D3, D4 and D5 are located approximately 550 m, 2000 m, and 100 m, respectively, northeast of the Site boundary (**Figure 5**). There is also one local residential well within 500 m of the Site that is screened in a sand gravel deposit located less than 30 mbgs. Residential water wells are a relatively low draw on the groundwater and given the thickness of the overlying till aquitard, is not expected to be affected by the proposed development.

## 5.0 Impact Assessment for Potential Receptors

The following section presents an evaluation of potential impacts on groundwater resources and surface water resources for the Site.

#### 5.1 Shallow Groundwater Features

Groundwater elevations across the Site are relatively shallow, generally less than 2 mbgs with levels close to surface in the spring. Water levels fluctuated on a seasonal basis. Groundwater levels near surface were noted in some wells during the spring season. Water levels generally follow ground surface elevations where the highest and lowest groundwater elevations were consistently observed within the northern and southern portion of the property, respectively. Interpreted groundwater flow direction is primarily in southwesterly direction along the west portion of the Site and a southeasterly direction along the east portion of the Site.

During the spring season, water level is hosted by the surficial sand, silty sand, and sand and gravel layer, and dropped into the underlying till unit in the drier period. The weathered till unit has an estimated hydraulic conductivity of  $3.8 \times 10^{-8}$  m/s. It is noted that there are no vertical groundwater movement within the till unit, and as such, this is considered a relatively impermeable material. Based on a review of the MECP WWR records, the till unit extends to approximately 35 mbgs. The hydraulic conductivity of the unweathered till aquitard is estimated at 7.6 x 10<sup>-10</sup> m/s, approximately 30 times lower than the weathered till.

Given that the till unit is relatively thick and is interpreted to be impermeable, there are no anticipated impacts to the underlying bedrock aquifer due to the proposed development.

To prevent leakage of groundwater into basements, it is anticipated that import fill is required to keep the basements above the high water table. It is understood that as a precaution, each basement will be designed to be surrounded by a foundation drain, which is considered normal practice within Township of Southgate. Typically, these are set to a minimum of 0.3 m above the measured high water table, assuming water levels could rise at some point in the future. The imported fill should be of the same hydraulic conductivity, or greater, than the native soil to prevent "wicking" up the water table to a higher elevation.

The design of the stormwater pond will have to consider the depth of the water table. Based on the groundwater elevations measured within the nested wells at MW7, there is negligible vertical groundwater movement. Instead, groundwater predominantly flows horizontally within the surficial sand, and silty sand till unit. With the aquifer soils conveying groundwater laterally, there is a danger of groundwater inflow occupying storage capacity of the SWM Pond. More importantly, the seepage has the potential to affect sidewall stability causing slumpage across the aquifer soils in the short to midterm. The results of this study should be reviewed by a Geotechnical Engineer to provide guidance on SWM Pond design.

#### 5.2 Potable wells

The Village of Dundalk relies on groundwater supply from wells screened within the dolostone bedrock that extends under the Site. The well capture zones have been documented by the Lake Erie Region Source Protection Committee and extend under the southeastern portion of the proposed development within the bedrock. The upper bedrock is inferred to be of low permeability, and the municipal production zone lies in the middle of the sequence. Municipal Wells D3, D4, and D5 are located approximately 550 m, 2000 m, and 1000 m, respectively, northeast of the Site.

However, given the thickness of the aquitard soils at this Site, and the fact that there will be no onsite sewage disposal through private septic beds, no impact to the groundwater quality in the aquifer is expected. Additionally, it is expected that pre-development recharge will have to be maintained in the post-development condition.

Rurally there are several surrounding individual residential private wells that tap into the dolostone bedrock and have been drilled to depths of approximately 26 mbgs to 113 mbgs. These residential water wells are a relatively low draw on the groundwater and given the thickness of the overlying aquitard, are not expected to be affected by the proposed development provided groundwater recharge is maintained.

Monitoring wells have been installed at the property as part of the Site-specific investigations to document stabilized groundwater conditions. Monitoring is on-going and is planned to continue through construction. When the monitoring wells are determined to be no longer required, or if they are determined to be at risk of damage from Site grading and construction, the wells should be properly decommissioned in accordance with O. Reg. 903. Decommissioning a well which is no longer in use helps ensure the safety of those in the vicinity of the well, prevents surface water infiltration into an aquifer via the well, prevents the vertical movement of water within a well, conserves aquifer yield and hydraulic head, and can potentially remove a physical hazard.

#### 5.3 Surface Water Features

A wetland/significant woodland is located in the southwest end of the Site, as well as a Willow Mineral Thicket Swamp. No significant upward groundwater springs are present, likely because the whole Site sits on a major topographic divide and there is no way to generate upward groundwater pressures. A fluctuating groundwater table helps sustains the vegetation, with the water levels within monitors MW22-406, MW22-407 and MW22-408, located adjacent to these wetland areas near or above surface in the wetter spring months. As the water table drops in the summer months, there is no groundwater contributions to the wetland. However, more porous sand and gravel soils are present at surface within the larger wetland/significant woodland, and is connected at depth to the wetland thicket. The sand and gravel unit is a pocket surrounded by surficial sandy silt till, and therefore has limited capacity to drain. Therefore, water collects within the glaciofluvial pocket and causes saturated conditions within the woodlot for extended periods of time throughout the year. It is anticipated that if the Site water balance is maintained by carefully implementing mitigation measures, the wetland will not be adversely affected by development of the Site.

## 6.0 Conclusion

The purpose of the Hydrogeological Assessment was to identify any hydrogeologic constraints to development. Based on the above results of the investigation and discussion, the following conclusions are presented.

- The Site is underlain by surficial sand to silty sand deposits up to 2 m thick. Underneath the surficial aquifer deposits is a sandy silt to silty sand till. The upper unweathered portion of the till unit has an estimated average hydraulic conductivity of 3.8 x 10<sup>-8</sup> m/s.
- The Site lies along a watershed drainage divide that runs through the centre of the Site in a north-south direction.
- Groundwater is interpreted to flow primarily in a southwesterly direction along the western portion of the Site and a southeasterly direction along the eastern portion of the Site.
- Currently, highest groundwater level conditions were recorded during the spring 2023 sampling event.
- No upward groundwater springs are present, likely because the whole Site sits on a major topographic divide and there is no way to generate upward groundwater pressures.
- Gas caps were installed at select monitors on March 7, 2024. To assess for the presence and temporal variability of soil gas concentrations, it is recommended that soil gas monitoring occurs at minimum, during periods of low water table (Summer 2024) and frozen conditions (Winter 2024/2025).
- It is recognized that portions of the Site are located within a WHPA, IPZ SGRA, and HVA. However, given the thickness of the till aquitard above the bedrock aquifer, there are no anticipated changes to the local water supply due to the proposed development.
- Municipal well D3, D4, and D5 are located approximately 550 m, 2000 m, and 1000 m, respectively, northeast of the Site. There are no anticipated hydrogeological impacts due to the proximal distance of the municipal wells to the proposed development area and thickness of the till aquitard below the Site.
- There are several surrounding individual residential private wells that are screened in the dolostone bedrock or overburden aquifer units. The residential water wells are a relatively low draw on the groundwater and given the thickness of the overlying clay aquitard, is not expected to be affected by the proposed development provided groundwater recharge is maintained.
- The wetlands in the southeastern portion of the Site are sustained by high groundwater levels in the spring, and residual moisture in the tension saturated zone above the water table in the drier months.
- The sand and gravel soils found in the southwestern portion of the Site are expected to contribute some lateral groundwater flow that serves to in part replenish water to the larger wetland/significant woodland. Provided the Site water balance is maintained the wetlands are not expected to be adversely affected by development of the Site.

## 7.0 Closure

We trust that this report satisfies your requirements at this time.

Regards,

SLR Consulting (Canada) Ltd.

allin Vuemi

Allison Vucenovic, M.Sc., G.I.T. Environmental Scientist

G MICHAELA. VENHUIS PRACTISING MEMBER 1061 024-05-06 NTAR

Michael Venhuis, M.Sc., P.Geo. Senior Hydrogeologist

Conta

Amanda Malatesta, M.Sc., P.Geo. Hydrogeologist

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## **Figures**

## Hydrogeological Assessment

Flato Ida

Flato Ida Dundalk Inc.

SLR Project No.: 209.30125.00001

May 6, 2024





































## Appendix A Development Plan

## Hydrogeological Assessment

Flato Ida

Flato Ida Dundalk Inc.

SLR Project No.: 209.30125.00001

May 6, 2024




N:\Southgate\752212 Ida Street, Dundalk — 15184AC\Drawings\Draft Plan\CAD\15184AC — Draft Plan — 2024—04—30.dwg

LAND USE	LOT / BLOCK #	UNITS	AREA
SINGLE DETACHED - 10.1m LOTS	001-266	266	9.454ha
TOWNHOUSE - 6.5m UNITS	267-278	52	1.218ha
FUTURE RESIDENTIAL	279	3	0.101ha
STORMWATER MANAGEMENT AREA	280, 281		2.558ha
SEWAGE PUMPING STATION	282		0.057ha
PARK	283, 284		2.002ha
OPEN SPACE	285		10.796ha
TOWNSHIP LANDS	286		5.011ha
COUNTY LANDS	287		0.065ha
0.3m RESERVE	288-292		0.003ha
FUTURE RIGHT OF WAY	293		0.065ha
RIGHT OF WAY	A, B, C, D, E, F, G		4.610ha
TOTALS		321	35.940ha



## Appendix B Borehole Logs

#### Hydrogeological Assessment

Flato Ida

Flato Ida Dundalk Inc.

SLR Project No.: 209.30125.00001

May 6, 2024



#### LIST OF ABBREVIATIONS AND DESCRIPTION OF TERMS

The abbreviations and terms commonly employed on the borehole logs and figures, and in the text of the report, are as follows:

#### SAMPLE TYPES

- AS Auger sample
- CS Chunk sample
- DO Drive open (split spoon)
- DS Denison type sample
- FS Foil sample
- RC Rock core (with size and percentage recovery)
- ST Slotted tube
- TO Thin-walled, open
- TP Thin-walled, piston
- WS Wash sample

#### **PENETRATION RESISTANCE**

Dynamic Cone Penetration Resistance:

A continuous profile showing the number of blows for each foot of penetration of a 2-inch diameter, 90° point cone driven by a 140-pound hammer falling 30 inches. Plotted as '—•—'

Standard Penetration Resistance or 'N' Value:

The number of blows of a 140-pound hammer falling 30 inches required to advance a 2-inch O.D. drive open sampler one foot into undisturbed soil. Plotted as ' $\Omega$ '

- WH Sampler advanced by static weight
- PH Sampler advanced by hydraulic pressure
- PM Sampler advanced by manual pressure
- NP No penetration

#### SOIL DESCRIPTION

**Cohesionless Soils:** 

<u>'N' (blov</u>	<u>ws/ft)</u>	Relative Density
0 to	4	very loose
4 to	10	loose
10 to	30	compact
30 to	50	dense
over	50	very dense

Cohesive Soils:

Undrai	ined	Shear				
Streng	<u>th (k</u>	<u>sf)</u>	<u>'N' (</u>	blov	vs/ft)	Consistency
less t	han	0.25	0	to	2	very soft
0.25	to	0.50	2	to	4	soft
0.50	to	1.0	4	to	8	firm
1.0	to	2.0	8	to	16	stiff
2.0	to	4.0	16	to	32	very stiff
0	ver	4.0	0	ver	32	hard

Method of Determination of Undrained Shear Strength of Cohesive Soils:

- x 0.0 Field vane test in borehole; the number denotes the sensitivity to remoulding
- $\triangle$  Laboratory vane test
- □ Compression test in laboratory

For a saturated cohesive soil, the undrained shear strength is taken as one half of the undrained compressive strength

#### METRIC CONVERSION FACTORS

1 ft = 0.3048 metres11b = 0.454 kg 1 inch = 25.4 mm1 ksf = 47.88 kPa



Soil Engineers Ltd.

GEOTECHNICAL • ENVIRONMENTAL • HYDROGEOLOGICAL • BUILDING SCIENCE

**PROJECT DESCRIPTION:** Proposed Buildings

PROJECT LOCATION: 752212 Ida Street, Township of Southgate (Dundalk)

METHOD OF BORING: Flight-Auger

Solid-Stem

DRILLING DATE: August 25, 2020



FIGURE NO.: 1

### JOB NO.: 2008-5025 LOG OF BOREHOLE NO.: BH/MW 2 FIGURE NO.: 2

**PROJECT DESCRIPTION:** Proposed Buildings

**METHOD OF BORING:** FI

DRILLING DATE: August 26, 2020

Flight-Auger Hollow-Stem

PROJECT LOCATION: 752212 Ida Street, Township of Southgate (Dundalk)



**PROJECT DESCRIPTION:** Proposed Buildings

EI.

(m)

Depth

(m)

512.5

0.0

<u>511.6</u> 0.9

506.1 6.4

END OF BOREHOLE

EARTH FILL

boulders

PROJECT LOCATION: 752212 Ida Street, Township of Southgate (Dundalk)

• Dynamic Cone (blows/30 cm) SAMPLES 10 30 50 70 90 Atterberg Limits Depth Scale (m) ΡL LL WATER LEVEL X Shear Strength (kN/m<sup>2</sup>) -SOIL 50 100 150 200 DESCRIPTION N-Value Number Penetration Resistance Ο Type (blows/30 cm) Moisture Content (%) 70 10 30 50 90 10 20 30 40 Ground Surface 25 cm TOPSOIL 0 47 1A DO 6 Ο 6 1B brown silty sand, trace of clay, some gravel, scattered topsoil 6 2 DO 10 Φ Brown, compact to very dense 1 Ā SILTY SAND TILL trace clay, some gravel to gravelly 511.3 m on completion occ. sand seams and layers, cobbles and 13 weathered 3 DO 13 О • 2 4 DO 29 Φ EI. Water Level @ 3 11 5 DO 0 25 4 8 50/15 6 DO • 5 6 8 7 DO 50/15 •

## Soil Engineers Ltd.

8

7

#### FIGURE NO .:

3

METHOD OF BORING: Flight-Auger

Solid-Stem DRILLING DATE: August 25, 2020

PROJECT DESCRIPTION: Proposed Buildings

PROJECT LOCATION: 752212 Ida Street, Township of Southgate (Dundalk)

METHOD OF BORING: Flight-Auger

Hollow-Stem

DRILLING DATE: August 25, 2020

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FIGURE NO.: 4

**PROJECT DESCRIPTION:** Proposed Buildings

METHOD OF BORING: Flight-Auger Solid-Stem

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FIGURE NO.: 5

### JOB NO.: 2008-5025 LOG OF BOREHOLE NO.: BH/MW 6 FIGURE NO.: 6

**PROJECT DESCRIPTION:** Proposed Buildings

METHOD OF BORING:

Flight-Auger Hollow-Stem

PROJECT LOCATION: 752212 Ida Street, Township of Southgate (Dundalk)

DRILLING DATE: August 24, 2020



### JOB NO.: 2008-S025 LOG OF BOREHOLE NO.: BH/MW 7S FIGURE NO.: 7A

PROJECT DESCRIPTION: Proposed Buildings

METHOD OF BORING: Flight-Auger

Hollow-Stem

PROJECT LOCATION: 752212 Ida Street, Township of Southgate (Dundalk)

DRILLING DATE: August 24, 2020

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					6 -								_			_	-			
					-					+		-					-			
					-											+	-			
					7 –															
					-															
					-					+					$\vdash$	+	-			
					8 -															
		Sc	oil	En	gin	ee	er	S	L	ta	<b>I</b> .						P	aue		1 of 1
	<b>V</b>																F'	uye	•	

### JOB NO.: 2008-S025 LOG OF BOREHOLE NO.: BH/MW 7D FIGURE NO.: 7B

**PROJECT DESCRIPTION:** Proposed Buildings

METHOD OF BORING: Flight-Auger

Hollow-Stem

**PROJECT LOCATION:** 752212 Ida Street, Township of Southgate (Dundalk)

DRILLING DATE: August 24, 2020



### JOB NO.: 2008-5025 LOG OF BOREHOLE NO.: BH/MW 8 FIGURE NO.: 8

**PROJECT DESCRIPTION:** Proposed Buildings

**METHOD OF BORING:** F

DRILLING DATE: August 26, 2020

Flight-Auger Hollow-Stem

PROJECT LOCATION: 752212 Ida Street, Township of Southgate (Dundalk)



	<b>\</b>  7		CLIENT: Flato Ida Dundalk	Inc.				В	OREH	OLE	ELOG	
	77	SLK	PROJECT: HydroG Assessm	ent					MW-	2	UTM COORDIN 4889927.94	IATES 42 N
SL	R CONSU	ILTING (CANADA) LTD.	SLR JOB NO: 209.30125.00001					SURFACE ELEVATION:	513.48 r	n	547803.8	43 E
	(m)			ЪЕ				TEST DATA		z Ū		(m)
(m)	NOI			1		very	Έ					NOT
PTH	EVAT	SO	IL DESCRIPTION	MPLI	MPLE	Seco	Ē			TER	COMPLETION	LA1
DE	ЕГЕ			SAI	SAN	% ⊦	so	■SPT Count ● % Mo	$50 \times 100$	S S	NOTES	ELE
	513.48	TOPSOIL	e medium sand trace roots. Dark		1A		<u>717</u> 71	♦ 33	.7		steel casing,	-
	515.25	brown, moist, soft.	e medium sand, trace roots. Dark	∕∖∖∖	40	65		■ 7			olionap, jpiag	F
		SAND			18			● 26.6				-513
-	512.72	Slity fine sand, trac	e medium sand, trace subangular vel. Brown with orange mottling.									Ī
1-	512.62	low plasticity, moist	, loose.	′  ▼	2	27	•		: : : : <del>:</del> ÷ ÷ ·			Ē
-		Silty fine sand trac	e medium and coarse sand trace		2	21				Ţ	<u>,</u>	[
-		subangular to subro	ounded gravel. Light brown, low							_	bentonite seal	_512
-		plasticity, moist, cor At 0.86 m, change t	mpact. to trace clay. Medium plasticity									512
-		wet.	to trade day. modiani practicity,	X	3	58		■ 4 ♦ 12.7				
2-												-
-												Ļ
	E40.04											-511
-	510.91 510.86	From 2.57 m to 2.6	2 m, cobble fragments.		4	75		■32 ♦ 9.4				-
		At 2.62 m, change f	to trace cobble. Moist.									ŀ
3-	510.43	At 3.05 m change t	to low plasticity wet dense									$\mathbf{F}$
		, a cree in, onange i			5	100		>50 🗰 🔶 10.8				ł
-											silian and	-510
-	509.82	SAND		-			ЩЩ				50mm 010 slot	-
	509 52	Medium and coarse	e sand, some subrounded gravel,								PVC pipe	ł
4-	000.02	trace fine sand, trac	ce silt. Brown, wet, loose.		6	100		>50	E			F
		Silty fine sand, trac	e medium and coarse sand, trace									F
	508.91	clay, trace subangu	lar to subrounded gravel, trace								end cap	-509
		At 4.57 m, change t	to greyish brown, medium	X	7	100		50 🔳 🔶 9.2				-
5-		plasticity.										T T
							•					Ī
	508.15	At 5.33 m. change t	to moist									-
-		, a croc m, change			8	100		>50 🔳 🔶 7.9				-508
-												
6-												Ī
-				Y	9	100		>50 🔳 🔶 8.2				
		End of borehole at	507.08 m							_		
		Woll Completion D	otoilo:									
		Screened interval fi	etalls: rom 510.58 m to 509.06 m									
		Elevation at top of p	pipe (TOP) = 514.30 m									
		Groundwater Inforn	nation:									
		Depth to groundwa	ter from TOP = 2.09 m (8/26/2020)									
1		Borehole backfilled	with drill cuttings moved over and									
		redrilled to desired	well depth and installed well.									
$\vdash$			Stem Auger Drilling				Teno					
	BOREHO	DIAMETER: 0.1016	5 m (OD)	NOTES		JPLI	1 370					
	DRILL DA	ATE: 2020 August 26	LOGGED BY: MW							She	et 1 of 1	
		-	DRILLED BY: Walker Drilling Ltd.							One		

SLR BOREHOLE LOG (MOISTURE) 241.20015.00005\_MW\_V4\_2023-05-05.0FJ SLR\_CAN V5.2 MOISTURE.GDT 23/5/5

	17		CLIENT:	Flato Ida Dundalk	Inc.						B	ORE	HO	LE	LOG	
	72	<b>SLK</b>	PROJECT: ADDRESS:	HydroG Assessme Flato Ida	ent				E	BOREH	OLE NO:	B⊢	I-5		UTM COORDIN 4890024.99	ATES 91 N
S		ILTING (CANADA) LTD.	SLR JOB NO	209.30125.00001		1			SURFA	CE EL	EVATION:	513.3	38 m		547910.67	71 E
DEPTH (m)	ELEVATION (m	SO	IL DESCRIPT	TION	SAMPLE TYPE	SAMPLE ID	% Recovery	SOIL TYPE	■SPT Co	Dunt	● % Moi	isture	BOREHOLE COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m
500005_MW_V4_2023-05-05.GPJ_SLR_CAN V5.2 MOISTURE.GDT_23/5/5 CAN V2.2 MOISTURE.GDT_23/5/5 CAN V5.2 MOISTURE.CDT_23/5/5 CAN V5.2 MOIS	NOLEY 313.38 513.38 513.15 512.96 511.09 511.09 509.57	SO TOPSOIL Fine sandy silt, trac SAND Silty fine sand, trac, subangular gravel, moist, compact. TILL Fine sandy silt, trac clay, trace subround brown, medium plas At 2.29 m, change t Moist, compact. From 3.31 m to 3.34 Wet. At 3.81 m, change t End of borehole at 3	IL DESCRIPT	TON brown, moist, soft. d, trace clay, trace ith orange mottling, d coarse sand, trace ular gravel. Light n. d, trace cobble. o fine sandy silt. wn.		Image: Control of the second secon	Linoopay % 100 13 85 100 100 100 100		■SPT C4 10 20 30 ■ 8 ■ 4 ■ 10 ■ 24	Dunt 40 50 ■ 4	<ul> <li>♦ % Mo</li> <li>20 40 60</li> <li>♦ 14.1</li> <li>♦ 10.7</li> <li>♦ 11.5</li> <li>● 9.8</li> <li>● 9.8</li> <li>● 9.8</li> <li>● 6.6</li> <li>● 6.8</li> <li>● 6.8</li> <li>● 6.9</li> </ul>	isture ) 80100 io.0	DESTROYON DESTROYON DESTROYON DESTROYON DESTROYON DESTROYON DESTROYON DESTROYON DESTROYON DESTROYON DESTROYON DE DESTROYON DESTROYON DE	WATER LEV	WELL COMPLETION NOTES         backfilled with drill cuttings	NOLENAJIJ -5113 -512 -512 -512 -511 - -510 - -509 - -508 - -508 - -
EHOLE LOG (MOISTURE) 241.200	DRILLING	G METHOD: Hollow	Stem Auger Drill	ing	Note	s:	SPLI	T SPO	ON							
BORE	BOREHO	LE DIAMETER: 0.1016		"'9 BY: MW	NOLES	5.	JF LI	1 350								
SLR	DRILL DA	TE: 2020 August 24	DRILLED	BY: Walker Drilling Ltd.										Shee	et 1 of 1	

	<b>V</b> 7		CLIENT: Flato Ida Dundalk	c Inc.			В	OREH	OLI	E LOG	
	- 24	'JLK	PROJECT: HydroG Assessm Address: Flato Ida	nent			BOREHOLE NO:	MW	-6	UTM COORDIN 4890069.8	ATES 22 N
S	LR CONS	ULTING (CANADA) LTD.	SLR JOB NO: 209.30125.00001				SURFACE ELEVATION:	514.77	m	547900.4	06 E
	L (E)			붠			TEST DATA		N		(m)
E (E		0.0			very	YPE			ШЦ ШЦ	WELL	10 1
PTH	EVA	30	IE DESCRIPTION	MPL MPL	Rec	- -	■SPT Count ●% Mo		MPI		EVA
B				sA SA	%	S S		<u>80 80100</u> ≥			Ш
	- 314.77	Fine sandy silt. trac	e roots. Dark brown, moist, soft.	1A			<b>◆</b> 26.6			steel casing, stickup, jplug	-
	514.36	SAND			75		■ 3				-
	+	Silty fine sand, trace	e medium sand, trace gravel.								-
	- 513.98	Brown, moist, comp	pact.	~ <b>\</b>		hit				,	-514
1	1	Fine sandy silt, trac	e clay, trace subrounded to	2	50	"	<b>5 12</b> .1			-	
	1	subangular gravel,	trace clay. Light brown, wet, firm.								
	513.25	At 1.52 m change t	to trace medium sand							bentonite seal	
			to trace medium sand.		83		<b>0</b>				-513
2	4				00	••••					-
	512.49										-
	512.40	At 2.29 m, change t	to silty fine sand, trace medium								-
	+	mottling, low plastic	city.	4	71		23 🔶 8.7				
	1										-512
3	511.70										
	] 011.05	Fine sand, trace me	edium and coarse sand,	5	82		■47♦ 9.7				
	1	laminations, wet, de	ided gravel. Light brown, horizontal ense.							silica sand	
	- 510.96	TILL				ļļļļļ				50mm 010 slot PVC pipe	-511
4	-	Silty fine sand, trace	e medium and coarse sand, trace ded to subangular gravel, trace	6A	100						-
	510.66	cobble. Light brown	with trace orange mottling,								-
	+	SAND	wei, compaci.	1						end cap	-
	- 510.20	Fine sand, trace me	edium sand, trace silt, occasional	7	92		>50 🔳 🔶 8.7		147 J		
	1	TILL									-510
5	1	Silty fine sand, trace	e medium sand, trace subrounded								
3/5/5	]	plasticity, wet, dens								backfilled with	-
DT 2		At 4.57 m, change t medium plasticity.	to trace clay. Greyish brown,	8	100		50 🖬 🔶 7.9			bentonite	-
RE.GI	-										-509
INIS 6	-							· · · · ·			-
	-	End of borobolo at	E00 E0 m	9	100	♥.	>50 🔳 🔶 8.8				-
I V5.2		End of borehole at	508.52 m								
CAN		Well Completion De	etails: rom 511 87 m to 510 35 m								
SLR		Elevation at top of p	pipe (TOP) = 515.54 m								
GPJ		Groundwater Inform	nation:								
5-05.		Depth to groundwat	ter from TOP = 1.72 m (8/26/2020)								
123-0											
4_20											
2											
05_0											
5.000											
2001											
241.											
JRE)											
DISTL											
D (MC											
ΓΟ											
			Stem Auger Drilling								<u> </u>
	BOREH	DLE DIAMETER: 0.1016	m (OD)	NULES.	OF LI						
SLR B	DRILL D	ATE: 2020 August 24	LOGGED BY: MW						Sh	eet 1 of 1	

	<b>V</b>		CLIENT:	Flato Ida Dundalk	Inc.						В	ORE	HC	)LE	LOG	
	7	<b>SLK</b>	PROJECT: ADDRESS:	HydroG Assessm Flato Ida	ent					BORE	HOLE NO:	M٧	N-7	7-D	UTM COORDIN/ 4889968.1	ATES 18 N
5		ISULTING (CANADA) LTD.	SLR JOB NO:	209.30125.00001		1			ડા	JRFACE E	LEVATION:	512.	05 m		547878.5	55 E
DEPTH (m)	ELEVATION (r	so	IL DESCRIPT	ION	SAMPLE TYPE	SAMPLE ID	% Recovery	SOIL TYPE	■SP	T Count	◆ % Mc	pisture	WELL COMPLETION	WATER LEVE	WELL COMPLETION NOTES	ELEVATION (r
	512.0 - 511.8 -	5 TOPSOIL 5 Fine sandy silt, trac SILT	e roots. Dark I	prown, moist, soft.		1A 1B	83		2	<u> </u>	◆ 19.4	48.1		Ţ	steel casing, stickup, jplug	-512 - -
1	511.4	<ul> <li>Sandy silt, trace cla mottling, moist, firm</li> <li>TILL</li> <li>Silty fine sand, trace</li> <li>subrounded to suba</li> <li>medium plasticity, n</li> </ul>	y, trace grave - e medium san angular gravel noist, compac	d, trace clay, trace Light brown,		2	33	•.	5		● 12.4					- - 511 -
2	510.5	At 1.52 m, change t At 1.70 m, change t plasticity.	o wet. o some grave	, trace cobble. Low		3	46	•.		17	<ul><li>◆ 8.1</li></ul>					- - -510
3	509.6	o SAND ○ Coarse sand, some trace medium sand, loose. TILL Silty fine sand, trace	subrounded t , trace fine sar	o subangular gravel, nd. Light brown, wet,		4A	83	•		34	<ul><li>◆13.4</li></ul>				bentonite seal	- - - -509
	508.2	4	, wet, compac	, frace clay, frace trace cobble. Light t.		5	78	•		>50	● 8.6					-
2		At 3.81 m, change t	o greyisn brov	vn.		6	92	•		50	. ♦ 8.6					-508 - -
23/5/5	- 507.2	<sup>8</sup> At 4.78 m, change t	o moist, dense	9.		7	100	•		>50	• 7.5				silica sand 50mm 010 slot	- -507 -
AOISTURE.GDT	506.4 506.1	1 <b>SAND</b> Fine sand, trace me subrounded gravel. compact.	edium sand, tra Light brown, i	ace silt, occasional non plastic, moist,		8A 9	100			>50    >50	<ul> <li>◆ 9.0</li> <li>→ 8.7</li> </ul>				end cap	- - -506
GPJ SLR_CAN V5.2 N		TILL Silty fine sand, trace subrounded to subro Greyish brown, low End of borehole at s Well Completion De	e medium san angular gravel plasticity, moi 505.78 m etails:	d, trace clay, trace trace cobble. st, dense.										<u> </u>		-
5_MW_V4_2023-05-05		Screened interval fr Elevation at top of p Groundwater Inform Depth to groundwat	om 507.45 m pipe (TOP) = 5 nation: er from TOP =	to 505.93 m 12.69 m - 1.08 m (8/26/2020)												
LOG (MOISTURE) 241.20015.0000																
HOLE	DRILI	ING METHOD: Hollow	Stem Auger Drilli	ng		 s: <b>\</b> _	SPI I	T SPC								
BORE	BORE	HOLE DIAMETER: 0.1016		SY: MW	NOLES	J. 1991		. 51 0								
SLR	DRILL	DATE: 2020 August 24	DRILLED E	SY: Walker Drilling Ltd.										She	et 1 of 1	

		17		CLIENT:	Flato Ida Dundalk	Inc.					BORE	HOL	ELOG	
	-		JLK	PROJECT: ADDRESS:	Flato Ida	ent				BOREH	OLE NO: M	W-7-8	UTM COORDIN 4889968.	ATES 18 N
		ONSUI	LTING (CANADA) LTD.	SLR JOB NO	209.30125.00001	ш				SURFACE EL	EVATION: 512 DATA	.07 m	547878.	55 E
лсрти <i>(</i> m)		ELEVATION	SO	L DESCRIPT	ΓΙΟΝ	SAMPLE TYF	SAMPLE ID	% Recovery	SOIL TYPE	•SPT Count	◆ % Moisture	WELL WELL COMPLETIO	WELL COMPLETION NOTES	ELEVATION
	512	2.07	For Lithology, see B	H7D borehol	e log.					10 20 30 40 50	20 40 00 80 10		steel casing,	-512
											·		silica sand 50mm 010 slot PVC pipe	- 511 - - - - 510 - - - - - - - - - - - - - - - - - - -
_;	3-		End of borehole at §	509.02 m									end cap	
LE LOG (MOISTURE) 241.20015.00005_MW_V4_2023-05-05.GPJ_SLR_CAN V5.2 MOISTURE.GDT_23/5/5			Well Completion De Screened interval fr Elevation at top of p Groundwater Inform Depth to groundwat	etails: om 510.70 m ipe (TOP) = { nation: er from TOP	to 509.17 m 512.74 m = 1.13 m (8/26/2020)									
REHOL		LLING	METHOD: Hollow S	Stem Auger Dril m (OD)	ling	Notes	:	-						
SLR BO	DRI	ILL DA	TE: 2020 August 25	LOGGED DRILLED	BY: MW BY: Walker Drilling Ltd.							Sh	eet 1 of 1	

CUCK       Process       File and the second part of the se	٦	CLIENT: Flato Ida Dunda	k Inc.				BORE	HOLI	E LOG	
BURCHARDELITING CANADA ITE:       S.R.JOG NO. 209.30125.00001       SUB FLACE ELEVATION.       513.94 m       947827888         Solid       SOLIDESCRIPTION       Image: Solid DESCRIPTION       Image: Solid	712	ADDRESS: Flato Ida	nent			BOREHOLE I	NO: MV	V-8	UTM COORDIN 4890027.2	IATES 64 N
general Solution       Solution	SLR CONSU	LTING (CANADA) LTD. SLR JOB NO: 209.30125.00001				SURFACE ELEVAT	ION: 513.6	4 m	547827.9	38 E
9:13.45 611.46 611.46 7.12       TOPEGOL. Tractum plasticly, most, soft. Sample and thrace day, trace roots. Dark brown, medium plasticly, most, soft. Sample and thrace day frame that have day. Sample and thrace day frame that have day. Fire and, trace medium mant, thrace day. Fire and, trace medium mant, trace day, trace Sample and trace medium mant sample and trace day. Sample and trace medium mant, trace day, trace Sample and trace medium mant, trace day, trace Sample and trace medium mant, trace day, trace Sample and trace medium mant, tra	DEPTH (m) ELEVATION (m)	SOIL DESCRIPTION	SAMPLE TYPE	% Recovery	SOIL TYPE	■SPT Count ◆9	A 6 Moisture	VELL COMPLETION VATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
Image: state series in the second set of the second set of the second secon	513.64	TOPSOIL	1A	<u>, 1</u>	<u>1</u> , <u>\</u>		<u>40 60 80100</u> ◆ 65.1		steel casing,	-
Pin the sain, face medium sain, face sourced         Pin the sain, face medium sain, face sourced         Pin the sain, face medium sain, face sourced         Pin the sain, face medium sain, face sourced         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face         Pin the sain, face medium sain, face day, tace         Pin the sain, face medium sain, face         Pin the sain, face medium sain, face         Pin the sain, face medium sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face         Pin the sain, face	- - 513.03 - 512.81 1- 512.75 -	SAND Sitty fine sand, trace medium sand, trace clay, occasional subrounded to subangular gravel. Brown with trace orange mottling, medium plasticity, moist, loose. TILL		58 29		■ 4 ■ 6 • 1	19.5 3.1		bentonite seal	- 513 - -
511.35       subcrounded to subangular gravel. Light brown, low         A1.2.25 m, change to trace cobble fragments. Dense.       A1.3.05 m, change to trace cobble fragments. Dense.         A1.3.05 m, change to dry. From 3.05 m to 3.20 m, hit       5         50.59       A1.3.05 m, change to dry. From 3.05 m to 3.20 m, hit       5         50.69       A1.3.05 m, change to dry. From 3.05 m to 3.20 m, hit       5         50.69       A1.3.05 m, change to dry. From 3.05 m to 3.20 m, hit       5         50.69       A1.3.05 m, change to dry. From 3.05 m to 3.20 m, hit       5         50.69       A1.3.05 m, change to dry. From 3.05 m to 3.20 m, hit       5         508.31       NOT RECOVERY       5         6       507.70       TitL       5         7       A3       50.9       6.8         9       9       6.8       5         9       7       A3       50.9       6.8         9       7       A3       50.9       6.8         9       9       6.8       5       5         9       7       A3       50.9       4.3         9       7       5       4.3       5         9       9       6.8       5       5         9       <	2-	to subangular gravel. Light brown, moist, compact. SAND Fine sand, trace medium sand. Brown, wet, compact TILL Silty fine sand, trace medium sand, trace clay, trace	3	46	<ul> <li>●.</li> </ul>	9	11			- -512 -
At 3.05 m, change to dry. From 3.05 m to 3.20 m, ht cobble layer. 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5	511.35 3- 510.59	subrounded to subangular gravel. Light brown, low plasticity, moist, compact. At 2.29 m, change to trace cobble fragments. Dense.	4	78	<ul> <li>▲</li> </ul>	>50 🔳 🔶	8		silica sand 50mm 010 slot PVC pipe	-511
a       7       83       7       83       50       6.5       50         508.31       NO RECOVERY       0       0       50       6.5       50         6       507.70       TLL       0       50       60       6.5       50         1       Stiff fire sand, trace medium sand, trace chay, trace       9       20       60       6.5       50         1       Stiff fire sand, trace medium sand, trace chay, trace       9       20       60       4.3         Subrounded to subangular gravel, trace cobble. Light       Vorm, low plastoly, dry, dense.       9       20       60       4.3         End of borehole at 507.49 m       Well Completion Details:       Screened interval from 511.66 m to 510.13 m       50       60       4.3         Groundwater Information:       Depth to groundwater from TOP = 4.24 m (8/26/2020)       Borehole backfilled with drill cuttings, moved over and redrilled to desired well depth and installed well.       Notes: Split SPOON       Split SPOON         DRILLINC METHOD:       Holew Stem Auger Drilling       Notes: Split SPOON       Split SPOON       NO RECOVERY         DRILLINC ELAMETER:       2006 wul28 d       LOCGED BY. MW       Notes: Split SPOON       Split SPOON	-	At 3.05 m, change to dry. From 3.05 m to 3.20 m, hit cobble layer.	5	100	•	50 <b>•</b> 7	.2		end cap	- - -51( -
908.31       NO RECOVERY       0       0       0       50	4- - - 5-		7	83	<ul> <li>●</li> <li>●</li> </ul>	>50	- <u>-</u>			- - -509 -
O       Utility fine sand, trace medium sand, trace clay, trace         Silty fine sand, trace medium sand, trace clay, trace         subrounded to subangular gravel, trace cobble. Light         brown, low plasticity, dry, dense.         End of borehole at 507.49 m         Well Completion Details:         Screened interval from 511.66 m to 510.13 m         Elevation at top of pipe (TOP) = 514.51 m         Groundwater information:         Depth to groundwater from TOP = 4.24 m (8/26/2020)         Borehole backfilled with drill cuttings, moved over and redrilled to desired well depth and installed well.         DRILLING METHOD:       Hollow Stem Auger Drilling         BOREHOLE DIAMETER:       0.1016 m (DD)         DRILLING METHOD:       Hollow Stem Auger Drilling         BOREHOLE DIAMETER:       0.1016 m (DD)         DRILL DATE:       200 404942 8	508.31					50 🖿				- 50
DRILLING METHOD:       Hollow Stem Auger Drilling         BOREHOLE DIAMETER:       0.1016 m (OD)         DRILL DATE:       2020 August 26		<b>NILL</b> Silty fine sand, trace medium sand, trace clay, trace subrounded to subangular gravel, trace cobble. Light brown, low plasticity, dry, dense.         End of borehole at 507.49 m         Well Completion Details:         Screened interval from 511.66 m to 510.13 m         Elevation at top of pipe (TOP) = 514.51 m         Groundwater Information:         Depth to groundwater from TOP = 4.24 m (8/26/2020)         Borehole backfilled with drill cuttings, moved over an redrilled to desired well depth and installed well.	)) d	25		50 - 4.	3			
DRILL DATE: 2020 August 26 LOGGED BY: MW		G METHOD: Hollow Stem Auger Drilling	Notes:		SPO	 ON				_
		LE DIAME I ER: 0.1016 m (OD) TE: 2020 August 26 LOGGED BY: MW		NO RE	COV	ERY				

SLR BOREHOLE LOG (MOISTURE) 241.20015.00005\_MW\_V4\_2023-05-05.GPJ SLR\_CAN V5.2 MOISTURE.GDT 23/5/5

	212		CLIENT:	Flato Ida Dundali	k Inc.						Mo	nitor	ing	W	ell LOG	
SI			ADDRESS:	Flato Ida 209 30125 00001	ICIIL				SU	BORE	HOLE NO:	ES	<b>5A-</b> 16 m	1		
	E E		OLNOOD NO.	200.00120.00001	PE					TEST			Z	VEL		(L)
DEPTH (m)	ELEVATION	SO	IL DESCRIPT	ON	SAMPLE TY	SAMPLE ID	% Recovery	SOIL TYPE	■SP7	Count	◆ % M	oisture	WELL	WATER LE	WELL COMPLETION NOTES	ELEVATION
	514.16	<b>TOPSOIL</b> Dark brown, organie	cs (rootlets), m	oist, soft		0-2.5	75.0	<u>1<sup>1</sup> - <sup>1</sup>11</u> <u>711<sup>1</sup> - <sup>1</sup>1</u>	<b>.</b> .5	00 40 0						-514
	513.73	Silty SAND TILL Fine-medium, brow	n, trace silt, so	ft, moist		0 2.0			T						bentonite seal	-
1-	-					*2.5-5	22.2									-
	-					DUP-1C	00.0							V		-513
	512.64	Silty SAND TILL Silty, light brown, gr dense, moist to dry	avel (sub-angi	ular), trace clay,		*5-7.5	70.8	•	12							-
2-	-							•								-512
	-					*7.5-10	50.0	•		>50					silica sand	-
3-	-					10-12.5	50.0	●.			49				50 mm 010 slot PVC pipe	-511
	-							•								-
4-	-					12.5-15	12.5			>50						-510
GDT 23/5/5	-					15-17.5	12.5	●.		>50				:	end cap	-
2 MOISTURE	-											· · · · · ·			bentonite seal	-509
SLR_CAN V5	-					17.5-20	50.0			>50						-
6-9		End of monitoring	(all at 500.00 m	_							<u> </u>					-
01_2023-05-0		Well Completion De Screened interval fr Elevation at top of r	etails: rom 512.64 m t pipe (TOP) = 5	to 509.59 m 15.16 m												
209.30125.000		Groundwater Inforn Depth to groundwat 2022)	nation: ter from TOP =	2.44 m (July 13,												
e log (moisture) <u>2</u>		* denotes soil samp	le taken for lal	o analysis												
		METHOD: Hollow	Stem Auger Drilli	ng	Note	s:	SPL	T SPC	ON	. : :						1
SLR BOI	DRILL DA	TE: 2022 April 13		SY: RH Y: Geo-Environmental										She	et 1 of 1	

	213	CLIENT: Flato Ida Dundali	Inc.					Monit	ori	ng	W	ell LOG	
SI		ADDRESS: Flato Ida SLR JOB NO: 209.30125.00001	GIIL						<b>MN</b> 518.6	<b>/2:</b> 0 m	2-4	01	
DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE ID	% Recovery	SOIL TYPE	■SPT Count 10 20 30 40 50	● % Moistu 20 40 60 80	Ire	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
	518.60	<b>TOPSOIL</b> Dark brown, organict (rootlets), soft, moist				$\frac{\sqrt{1}}{1} \frac{\sqrt{1}}{\sqrt{1}} \frac{\sqrt{1}}{\sqrt{1}}$			2100			silica sand	-
	518.32	SAND Fine-medium, some gravel, some silt, brown, soft, moist		0-2.5	45.8		4						- -518
1-	-			*2.5-5	33.3		8						-
2-	-			*5-7.5	50.0		8						-517 - -
	516.31	Silty SAND TILL Silty fine sand, gravel (sub-angular/sub-rounded), orange mottling, light brown, dense, dry		7.5-10	83.3	•	33					bentonite seal	-516
3-	•			10-12.5	75.0	•.	4	8			Ţ		- - -515
4-	514.79	No orange mottling, wet, loose		12.5-15	58.3	•.							-
5-	+ - -			15-17.5	29.2	•.	>50		-			silica sand 50 mm 010 slot	-514 - -
6-	-			17.5-20	0	•.	>50 🖿					PVC pipe	- -513 -
		End of monitoring well at 512.50 m								<u>: [];</u> ;		<mark>⊦end cap</mark>	
		Well Completion Details: Screened interval from 514.03 m to 512.50 m Elevation at top of pipe (TOP) = 519.50 m											
		Groundwater Information: Depth to groundwater from TOP = 4.28 m (July 13, 2022)											
		* denotes soil sample taken for lab analysis											
		G METHOD: Hollow Stem Auger Drilling	Notes	s: 🔼	SPL	T SPC	ON	: : : :	_:   		1		
-	DRILL DA	ATE: 2022 April 13 LOGGED BY: RH									Sha	et 1 of 1	
		DRILLED BY: Geo-Environmental									Sile		

		212		CLIENT:	Flato Ida Dundal	k Inc.						Μ	onito	ori	ng	W	ell LOG	
				ADDRESS:	Flato Ida	nent							ר: <b>N</b>	<b>///</b>	<b>/2</b>	2-4	102	
		E E	LTING (CANADA) LTD.	SLR JUB NU	209.30123.00001	Щ				5	TEST		<u>, N: J</u>		z	Ē		E)
DEPTH (m)		ELEVATION	SO	IL DESCRIPT	ION	SAMPLE TYI	SAMPLE ID	% Recovery	SOIL TYPE	■SF	PT Count	◆% 204	Moistu	re 100	WELL COMPLETIC	WATER LEV	WELL COMPLETION NOTES	ELEVATION
	5	16.82	TOPSOIL Brown, moist, soft			X	0-1	50.0	<u>x11/ x1</u> 1/ x1/	<b>–</b>	15						silica sand	-
1	5	16.52	Silty SAND TILL Silty, gravel (sub-an brown, moist, soft-d with depth	igular), trace ( ense, increas	clay, some organics, ing gravel content		2.5-3.0	45.8		5				· · · · · · · · · · · · · · · · · · ·				- 516 -
2	2-					X	5.5-6.5	83.3	•		15			·····		Ţ	bentonite seal	- 515 -
3	3-						7.5-10	100.0	<ul><li>▲.</li></ul>		>50			•••••••••••••••••••••••••••••••••••••••				- 514 -
2	+					X	11-12	79.2	<ul><li>●.</li></ul>		>50 🗖			•••••••••••••••••••••••••••••••••••••••				- -513
/5							14-15	50.0	• •.		>50							- - -512
TURE.GDT 23/5	-					X	17-17.5	33.3	•		>50 🗖						silica sand 50 mm 010 slot PVC pipe	-
CAN V5.2 MOIS	3-						18-20	100.0	•		>50						end cap silica sand	-511
-05.GPJ SLR			End of monitoring w	vell at 509.96	m		20.5-22	.587.5			>50 🗖						bentonite seal	510
0001_2023-05			Well Completion De Screened interval fr Elevation at top of p	etails: om 512.25 m vipe (TOP) = {	to 510.72 m 17.68 m													
URE) 209.30125.(			Groundwater Inform Depth to groundwat 2022)	nation: er from TOP	= 2.95 m (July 13,													
OLE LOG (MOIST			* denotes soil samp	le taken for la	b analysis													
OREH(	DF BC	RILLING	METHOD: Hollow S LE DIAMETER: 0.2 m (0	Stem Auger Drill OD)	ing	Notes		SPLI	T SPC	ON								
SLRB	DF	RILL DA	TE: 2022 April 11	LOGGED DRILLED	BY: RH 3Y: Geo-Environmental											She	et 1 of 1	

	<u></u>		CLIENT: Flato Ida Dunda	lk Inc.					Mon	itori	ing	W	ell LOG	
	22	JLK	PROJECT: HydroG Assessi Address: Flato Ida	ment				BORE	HOLE NO:	MV	V2	2-4	-03	
S		JLTING (CANADA) LTD.	SLR JOB NO: 209.30125.00001					SURFACE EL	EVATION:	514.2	27 m	۱ . ا ـــا		Ê
DEPTH (m)	ELEVATION (r	SO	IL DESCRIPTION	SAMPLE TYP	SAMPLE ID	% Recovery	SOIL TYPE	■SPT Count 10 20 30 40 50	◆ % Moi	sture 80100	WELL COMPLETION	WATER LEVE	WELL COMPLETION NOTES	ELEVATION (r
	514.27	TOPSOIL _ Dark brown, some of	organics (rootlets), soft, moist				$\frac{\sqrt{1}}{1}, \frac{\sqrt{1}}{1}$						silica sand	-
	-	SAND Fine-medium, brow	n, trace clay, soft, moist		1-2.5	66.7		■ 4						-514
1		Sandy SILT TILL Silty, light brown, gr soft, moist, increasi	ravel (sub-angular), trace clay, ng gravel content with depth		455	20.8	•.							- 513
2	-			Y	6.5-7.5	37.5	•.	24				Ţ		-
	511.98	Cobbles, dry, dense	9			0.10	<ul><li>●.</li></ul>						bentonite seal	-512
3	-				9-10	66.7	<ul><li></li><li></li><li></li><li></li><!--</td--><td></td><td></td><td></td><td></td><td></td><td></td><td>-511</td></ul>							-511
4	-				11.5-12	2.5 58.3	•	>50						
	-				14-15	62.5	•	>50						-
URE.GDT 23/5/5	508.94	Moist from 5.33 m t	o EOH		16.5-17	.5 <sup>50.0</sup>	•.	>50 🗖					silica sand 50 mm 010 slot PVC pipe	-509
CAN V5.2 MOIST	-				19-20	66.7	◆.	>50 🛛					end cap silica sand	- - -508
GPJ SLF	507.49	- Largest cobble at 6	78 m	X	22-22.5	5 37.5		>50					bentonite seal	-
05-05		End of monitoring w	vell at 507.41 m	-/										
.00001_2023-		Well Completion De Screened interval fr Elevation at top of p	etails: rom 509.70 m to 508.17 m pipe (TOP) = 515.21 m											
IRE) 209.30125.		Groundwater Inforn Depth to groundwat 2022)	nation: ter from TOP = 2.79 m (July 13,											
E LOG (MOISTU		* denotes soil samp	ble taken for lab analysis											
	DRILLING	G METHOD: Hollow	Stem Auger Drilling	Notes	 s: <b> </b>	SPL	I T SPC	ION	1 : : :	<u>: : </u>				
BOR	BOREHO	DLE DIAMETER: 0.2 m (	OD) LOGGED BY: RH	-										
SLF	DRILL DA		DRILLED BY: Geo-Environmental									She	et 1 of 1	

	212	CLIENT: Flato Ida Dundalk	Inc.				Monito	orin	g W	lell LOG	
e1			ent				BOREHOLE NO: N	1W2	2 <b>2-4</b>	404	
51		DETING (CANADA) LID. SLR JOB NO: 209.30123.00001	Ы				TEST DATA	14.101	ਸ ਟ ਦਿ		E)
DEPTH (m)	ELEVATION	SOIL DESCRIPTION	SAMPLE TY	SAMPLE ID	% Recovery	SOIL TYPE	■SPT Count ◆ % Moistur 10 20 30 40 50 20 40 60 80	well	COMPLETIC WATER LEV	WELL COMPLETION NOTES	ELEVATION
	514.16 513.96	TOPSOIL				<u>74 1<sup>×</sup> 71</u>				silica sand	-514
		SAND Brown, some silt, organics, (rootlets), moist, soft		0-2.5	66.7		<b>₩</b> .4				-
- 1- -	513.40	Silty SAND Medium sand, brown, orange mottling, gravel (sub-angular/angular), soft, compact, wet		*2.5-5 / DUP-1B	66.7		12		Ţ		- - 513
2-	512.64	Silty SAND TILL Medium-fine silty sand, some gravel (sub-angular/angular), compact/dense, wet		*5-7.5	75.0		<b>4</b> 4				-
-	511.87									bentonite seal	-512
-			С	)	0		>50 🗖				-
3-	511.11	<b>Gravelly SAND</b> Grey-brown, gravel (sub-angular/angular), some silt, wet, loose		10-12.5	91.7	° 0	>50 📭				- -511 - -
- 4- -	510.30	Silty SAND TILL Silty fine sand, gravel (sub-angular/angular), grey-brown, dry, dense		12.5-15	66.7		>50 🖬				- - -510 -
- - 5-				15-17.5	54.2	•	>50 🖬			silica sand	- - - -509
-				17.5-20	70.8	<ul><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li><li></li></ul>	>50 🔳			PVC pipe	-
-0				20-22.5	0	•	>50			end cap silica sand bentonite seal	508 - -
		End of monitoring well at 507 20 -									-
		Well Completion Details: Screened interval from 509.59 m to 508.06 m Elevation at top of pipe (TOP) = 515.00 m									
		Groundwater Information: Depth to groundwater from TOP = 1.77 m (July 13, 2022)									
		* denotes soil sample taken for lab analysis									
	DRILLIN	G METHOD: Hollow Stem Auger Drilling	Note	s: 🔼 🔅	SPI I	T SPC	 DON	:			
	BOREHO	DLE DIAMETER: 0.2 m (DD)	NOLES		NO F	RECO	/ERY				
	URILL D	ATE: 2022 April 13 DRILLED BY: Geo-Environmental							She	eet 1 of 1	

SLR BOREHOLE LOG (MOISTURE) 209:30125.00001\_2023-05-05.0FJ SLR\_CAN V5.2 MOISTURE.GDT 23/5/5

	<u>\</u>	<u>, 1 – 1</u>		CLIENT: Flato Ida Dundalk	Inc.						Mo	nitor	ing	W	ell LOG	
•				ADDRESS: Flato Ida	ent				<b>Q</b> 11		IOLE NO:	512	<b>V2</b>	2-4	05-D	
3		Ê	LING (CANADA) LID.	SER JOB NO. 203.30 123.0000 1	Щ		Γ		- 30	TEST		012.	z	:		Ê
DEPTH (m)	EI EVATION	ELEVATION	SOI	L DESCRIPTION	SAMPLE TYF	SAMPLE ID	% Recovery	SOIL TYPE	■SP1	Count	◆ % M	oisture 50 80100	WELL COMPLETIO	WATER LEV	WELL COMPLETION NOTES	ELEVATION
	512 511	2.10 .87 -	TOPSOIL	s (rootlets) moist soft	_			<u>7, 1<sup>×</sup> 7</u>						÷.	silica sand	-512
	1		SAND			1 5-2 5	70.8									-
	511	.34	Medium sand, light t	prown, organics (rootlets), moist,		*2.5-5										-
			Silty fine sand with g moist, soft	gravel (sub-angular), light brown,		/ DUP-1A	58.3		9			<u> </u>				-511 -
	510	).58  -	Silty SAND with GR	AVEL		*5 7 5	37.5	0	12							-
2	-		light brown, moist-dr	y, soft		5-7.5	57.5	0						-		- 510
	]					<b> </b>		0								-
	1					7.5-10	75.0	0		22						-
3	509	0.05	☐ Gravelly SAND			1					1	<u>+ + -</u> ·				-509
			Coarse sand and gra sand, trace silt, light Silty SAND TIL	avel (sub-angular), some fine brown, wet, loose		10-12.5	66.7	•.		>50						-
4			Silty fine sand with g light brown-grey, dry	ravel (sub-angular), trace clay, v, dense		12.5-15	79.2	•		 >50 ∎						-508
								•.							bentonite seal	-
5					X	15-17.5	66.7			>50 🔳		<u> </u>				-
	+															-507
	1				Y	17.5-20	45.8			>50						
6	-							•••								-
	1					20.22.5	27 5			>=0 <b>•</b>						-506 -
	]					20-22.5	57.5			>50 <b>•</b>						_
7	1											÷ ÷ ÷				-
5/5					Å	2.5-25	87.5			50						-505
T 23/	+					1										-
8 KE	-				X	25-27.5	70.8			<u>&gt;50</u>		<u> </u>				- -504
DISTU	1							•								
5.2 MC					X	27.5-30	58.3			>50 🔳						-
9 NA	-								<u> </u>		+	$\frac{1}{1}$ $\frac{1}{1}$ $\frac{1}{1}$				-503
SLR_(	+				$\bigcirc$		0	●.		>50 🔳						-
GPJ	1														silica sand	-
50 10 50	1					32.5-35	0				+ 17	<u></u> .			PVC pipe	-502
2023-	1															F
00001			End of monitoring w	ell at 501.43 m											end cap	
9.30125.(			Well Completion De Screened interval fro Elevation at top of p	tails: om 502.96 m to 501.43 m ine (TOP) = 513.05 m												
<u>RE) 2(</u>			Groundwater Inform	ation:												
ISTUF			Depth to groundwate	er from TOP = 2.81 m (July 13,												
G (MC			20221													
μĹ			* dopotes '' '	a takan far lah arahati												
	DRIL		METHOD: Hollow S	Stem Auger Drilling	Votes		SPL	T SPO	ON	<u> </u>	1 : :	<u>: : :</u>	I			
3 BOR	BOR		E DIAMETER: 0.2 m (0	DD) LOGGED BY: RH		$\Box$	NO F	RECO	'ERY					<u> </u>		
S	DRIL			DRILLED BY: Geo-Environmental										She	et 1 of 1	

DEPTH (m)	E CONSU (E) NOLLEY NOLLEY NOLLEY S112.06 5111.83	LTING (CANADA) LTD.	PROJECT: Hydrog Assessmi ADDRESS: Flato Ida SLR JOB NO: 209.30125.00001 DESCRIPTION					BO	REHOLE NO	D: M	N2	2-4	05-S	
	(E) NOILEVAU 312.06 511.83	SOIL I	DESCRIPTION	гуре		-								
DEPTH (m)	NOLEA BIE 512.06 511.83	SOIL	DESCRIPTION	17				TF	EST DATA	<u>/N:</u> J1Z.	z	Ш		Ê
-	512.06 511.83			SAMPLE 1	SAMPLE ID	% Recovery	SOIL TYPE	■SPT Cou	nt ♦%	Moisture 0 60 80100	WELL COMPLETIO	WATER LEVI	WELL COMPLETION NOTES	ELEVATION
	511.83	TOPSOIL Dark brown, organics	(rootlets), moist, soft				<u>x11/ x1</u>						silica sand	-512
1-		SAND Medium sand, light bro soft	own, organics (rootlets), moist,		1.5-2.5	70.8		<b>4</b>			•			
	511.30	Silty fine sand with gra moist, soft	avel (sub-angular), light brown,		*2.5-5 / DUP-1A	58.3		9						- 511 -
2-	510.54	Silty SAND with GRAN Silty fine sand with gra light brown, moist-dry,	<b>/EL</b> avel (sub-angular), trace clay, soft		*5-7.5	37.5	0 0 0 0 0 0	12				Ţ		- - -510
	509.01				7.5-10	75.0	0 0 0 0	22					bentonite seal	
-	508.95	Gravelly SAND Coarse sand and grav sand, trace silt, light bu Silty SAND TILL Silty fine sand with gra light brown-grey, dry, o	rel (sub-angular), some fine rown, wet, loose avel (sub-angular), trace clay, dense		10-12.5	66.7	•	>5	0					-
4-					12.5-15	79.2	<b>●.</b>	>5	0					-508 - -
					15-17.5	66.7	<ul><li>●.</li></ul>	>5	0				silica sand 50 mm 010 slot PVC pipe	-507
					17.5-20	45.8	•	>5	D <b>II</b>				and con	- - 506
		End of monitoring well Well Completion Deta Screened interval from Elevation at top of pipe	l at 505.96 m ils: n 507.49 m to 505.96 m e (TOP) = 513.05 m										···•	
		Groundwater Informat Depth to groundwater 2022)	ion: from TOP = 2.79 m (July 13,											
		* denotes soil sample MW22-405S was strai MW22-405D	taken for lab analysis ight drilled adjacent to											
5 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		METHOD: Hollow Ste	em Auger Drilling	Notes		SPLI	T SPO	ON		<u>:::</u> :	L			1
	DRILL DA	TE: 2022 April 12	LOGGED BY: RH									She	et 1 of 1	

	22			Flato Ida Dundal	k Inc. nent						Мо	nitor	ing	W	ell LOG	
SI			ADDRESS:	Flato Ida 209.30125.00001	iont				SI	BOREH	HOLE NO:	<b>M</b> 1: 511.	<b>N2</b> 50 m	2-4	106	
	<u><u> </u></u>				ЪЕ					TEST	DATA	•	Z	/EL		r (m)
DEPTH (m)	ELEVATION	SO	IL DESCRIPT	ION	SAMPLE TY	SAMPLE ID	% Recovery	SOIL TYPE	■SP <sup>-</sup>	T Count	◆% N 2040	loisture 60 80100	WELL COMPLETIC	WATER LEV	WELL COMPLETION NOTES	ELEVATION
	511.50 511.40	<b>TOPSOIL</b> SAND Fine sand, trace silt mottling, moist, soft	t, trace organie , loose	cs, brown, grey		0-2.5	66.7	<u>x 1</u> /2 <u>x</u>	4						cement	- - -511
1-	510.74	Silty SAND Grey, brown mottlin cobbles, moist, firm	g, silty, trace ( , compact	gravel, trace clay,		2.5-5	62.5		5					Ţ		-
2-	-					5-7.5	54.2		9			· · · · · · · · · · · · · · · · · · ·			bentonite seal	- 510
3-	509.21	Silty SAND and GR Brown-grey, silty, gr Dry	<b>AVEL</b> ravelly, moist,	firm, compact		7.5-10	100.C	0 0 0 0		■ 36						- -509 -
	507.69	GRAVEL				10-12.5	100.C	0		∎ 35						- 508 -
-4-	506.93	Brown-grey, crushe saturated, loose	d rock/gravel	(angular), trace silt,		12.5-15	41.7			40						- - -507
AN V5.2 MOISTURE	506.78	Brown, gravel, satu GRAVEL Brown, angular, trad loose	rated, loose ce fine sand, t	race cobble, wet,		15-17.5	54.2					· · · · · · · · · · · · · · · · · · ·			silica sand 50 mm 010 slot PVC pipe	-
	506.17	Silty SAND TILL Brown-grey, silty, so	ome gravel, di	y, dense		17.5-19	66.7			>50					end can	-506
. LOG (MOISTURE) 209.30125.00001_2023-05-(		End of monitoring w Well Completion De Screened interval fr Elevation at top of p Groundwater Inform Depth to groundwat 2022) * denotes soil samp	vell at 505.71 etails: rom 507.23 m bipe (TOP) = 5 nation: ter from TOP : ble taken for la	m to 505.71 m ;12.31 m = 1.92 m (July 13, b analysis												
		G METHOD: Hollow	Stem Auger Drill	ing	Note	s: 🔼	SPL	 T SPC	ON							
	BOREHC	DLE DIAMETER: 0.2 m (	OD) LOGGED	BY: MJ										<u> </u>		
<u></u>			DRILLED I	BY: Geo-Environmental										She	et 1 of 1	

	22		CLIENT: Flato Ida Dundalk	Inc.					Mon	itori	ing	W	ell LOG	
SI			ADDRESS: Flato Ida	5110				BOREH SURFACE FL	IOLE NO: EVATION <sup>.</sup>	MV 509.0	<b>V2</b> 51 m	2-4	07	
(m)	(m) NOI			E TYPE	0	very	ЪЕ	TEST	DATA		ETION	LEVEL		(m) NOI
DEPTH	ELEVAT	SO	IL DESCRIPTION	SAMPLE	SAMPLE	% Reco	SOIL TY	■SPT Count 10 20 30 40 50	♦ % Mo 20 40 60	isture ) 80100	WELL	WATER	COMPLETION NOTES	ELEVAT
	509.61	TOPSOIL					$\frac{\sqrt{h_2}}{\sqrt{h_2}}$						cement	[
	509.38	<b>Silty SAND</b> Brown, silty, trace c	cobble, moist, soft		0-2.5	37.5		7						-
	-													-509
1-					2.5-5	16.7		<b>6</b>	+					-
	508.09	Occasional gravel	compact									V		-
	-	<u> </u>			5-7.5	70.8		12				-		
2-	507.32								+				bentonite seal	-
		Sandy SILT TILL Grey-brown, gravell dry-moist, firm, com	ly (sub-angular/angular), trace silt, ıpact		7.5-10	83.3	●.	>50 🖿						-507
3-							•							-
	-				10-12 5	41.7	●.	>50						-
							•							-506
4-	-						●.							-
	-				12.5-15	100.0		>50				· .		-
17 23/5/5	-				1		●.							-505
STURE.GD					15-17.5	95.8		>50 🗰						
V5.2 MOIS					1		•.						silica sand 50 mm 010 slot PVC pipe	-
SLR_CAN	+				17.5-20	70.8		>50 🔳						-504 -
-02.GPJ .	+	End of monitoring v	vell at 503.51 m										end cap	-
01_2023-05		Well Completion De Screened interval fr Elevation at top of r	etails: rom 505.04 m to 503.51 m ope (TOP) = 510.46 m											
9.30125.000		Groundwater Inform Depth to groundwat	nation: ter from TOP = 2.46 m (July 13,											
-URE) 20(		20221												
OG (MOIST		* denotes soil samp	ble taken for lab analysis											
		G METHOD: Hollow	Stem Auger Drilling	Notes	s: 💌	SPL	T SPO	ON						
R BOR	BOREHO	DLE DIAMETER: 0.2 m (	OD) LOGGED BY: MJ									<u> </u>		
			DRILLED BY: Geo-Environmental									She	et 1 of 1	

	217	CLIENT: Flato Ida Dundalk	Inc.				Monit	ori	ng	W	ell LOG	
SL		DILTING (CANADA) LTD. PROJECT: HydroG Assessme ADDRESS: Flato Ida SLR JOB NO: 209.30125.00001	ent				BOREHOLE NO:	<b>MN</b> 509.3	<b>/22</b> 1 m	<u>2</u> -4	-08	
DEPTH (m)	ELEVATION (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE ID	% Recovery	SOIL TYPE	TEST DATA • SPT Count 10 20 30 40 50 20 40 60 8	ure 0100	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
-	509.31 509.18	TOPSOIL Silty SAND with GRAVEL Brown, silty, some gravel, trace clay, trace organics, moist-wet, occasional cobbles, loose-dense, increasing gravel content with depth		*0-5	100.0		■ 5				cement	509
1-						0 0 0				Ţ		- 508 -
2-	507.02	Saturated, hard, compact		5-7.5	45.8	0 0	• 9 				bentonite seal	- - -507
3-	506.26	Set, very hard, very dense		*7.5-10	70.8	0 0 0 0 0 0						-
				10-12.5	75.0	0 0 0 0	>50					-506
4-				12.5-15	70.8	0 0 0	 >50 <b>0</b>					- 50: -
5-	503.98	Gravelly Silty SAND		15-17.5	37.5	0 0 0	>50 💵				silica sand 50 mm 010 slot PVC pine	504
6-		Brown-grey, moist-wet, dense, soft		17.5-20	62.5	0 0 0	>50 🗖				end cap	-
· ·				20-22.5	16.7	9 0 0 0	>50 🔳				silica sand bentonite seal	-503 - -
		End of monitoring well at 502.45 m Well Completion Details: Screened interval from 504.74 m to 503.21 m Elevation at top of pipe (TOP) = 510.28 m										
		Groundwater Information: Depth to groundwater from TOP = 2.18 m (July 13, 2022)										
		* denotes soil sample taken for lab analysis										
	DRILLING BOREHO	6 METHOD: Hollow Stem Auger Drilling LE DIAMETER: 0.2 m (OD)	Notes		SPLI	T SPO	ON	<u> </u>			,	
	DRILL DA	TE: 2022 April 18 DRILLED BY: Geo-Environmental								She	et 1 of 1	



## Appendix C Groundwater Data

#### Hydrogeological Assessment

Flato Ida

Flato Ida Dundalk Inc.

SLR Project No.: 209.30125.00001

May 6, 2024



Table C-1:	Groundwater	<b>Elevations</b>	in Monitoring	Wells
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Monitor ID	Units	25-Sep-20	16-Nov-20	5-Apr-21	5-Jul-21	9-Sep-21	3-Nov-21	13-May-22	13-Jul-22	20-Sep-22	25-Nov-22	28-Mar-23	1-Nov-23	7-Mar-24
ESA_1	mbgs	-	-	-	-	-	-	0.79	1.46	1.72	1.16	0.54	-	0.64
LOAT	masl	-	-	-	-	-	-	513.37	512.70	512.44	513.00	513.62	-	513.52
MW22 401	mbgs	-	-	-	-	-	-	2.40	3.38	3.86	3.63	0.89	-	1.25
1010022-401	masl	-	-	-	-	-	-	516.20	515.22	514.74	514.97	517.72	-	517.35
MW22 402	mbgs	-	-	-	-	-	-	1.37	2.09	3.29	3.19	0.14	-	0.55
1010022-402	masl	-	-	-	-	-	-	515.45	514.73	513.54	513.64	516.69	-	516.27
MW22 403	mbgs	-	-	-	-	-	-	0.89	1.85	2.61	1.40	0.20	-	0.28
1010022-403	masl	-	-	-	-	-	-	513.38	512.42	511.66	512.87	514.07	-	513.99
M\\/22_404	mbgs	-	-	-	-	-	-	1.14	0.93	2.31	1.40	0.36	-	0.43
1010022-404	masl	-	-	-	-	-	-	513.02	513.23	511.85	512.76	513.80	-	513.73
MW/22 405 S	mbgs	-	-	-	-	-	-	0.81	1.80	2.55	1.82	0.04	0.56	0.09
1010022-405-5	masl	-	-	-	-	-	-	511.25	510.26	509.51	510.24	512.02	511.50	511.97
MW/22 405 D	mbgs	-	-	-	-	-	-	0.85	1.86	2.63	1.91	0.11	0.69	0.22
WW 22-405-D	masl	-	-	-	-	-	-	511.25	510.24	509.47	510.20	511.99	511.41	511.88
MW22 406	mbgs	-	-	-	-	-	-	0.33	1.11	1.76	0.93	0.11	0.48	0.15
1010022-400	masl	-	-	-	-	-	-	511.17	510.39	509.74	510.57	511.39	511.02	511.35
MW22 407	mbgs	-	-	-	-	-	-	-0.44	1.51	2.34	1.21	0.15	-	0.18
1010022-407	masl	-	-	-	-	-	-	509.95	508.00	507.17	508.30	509.37	-	509.33
MW22 408	mbgs	-	-	-	-	-	-	0.33	1.21	1.23	0.12	0.07	0.07	0.07
1010022-408	masl	-	-	-	-	-	-	508.98	508.10	508.08	509.19	509.24	509.24	509.24
	mbgs	1.17	0.76	0.96	1.27	1.07	0.93	1.11	1.71	2.41	1.92	0.73	-	0.88
DH-2	masl	512.32	512.72	512.52	512.22	512.41	512.56	512.37	511.77	511.07	511.56	512.75	-	512.60
RH 6	mbgs	0.64	0.03	0.10	0.51	0.21	0.09	0.51	1.36	1.84	1.26	0.15	0.82	0.20
ВП-0	masl	514.13	514.74	514.67	514.26	514.56	514.69	514.26	513.41	512.93	513.51	514.62	513.96	514.57
	mbgs	0.25	-0.01	0.02	0.12	0.01	-0.02	-	0.45	0.73	0.05	0.02	0.05	0.03
вп-7-3	masl	511.82	512.08	512.05	511.95	512.06	512.09	-	511.62	511.35	512.02	512.06	512.02	512.04
	mbgs	0.22	0.00	0.01	0.22	-0.01	-0.02	0.14	0.58	0.72	0.04	0.00	0.03	0.03
U-1-D	masl	511.83	512.05	512.04	511.83	512.06	512.07	511.91	511.47	511.33	512.01	512.05	512.02	512.02
р <b>ц</b> о	mbgs	0.47	-0.03	0.01	0.22	0.01	0.01	0.31	0.90	1.23	0.53	-0.02	-	-0.01
DI1-0	masl	513.17	513.67	513.63	513.42	513.63	513.63	513.33	512.74	512.41	513.11	513.66	-	513.65

Notes: mbgs metres below ground surface

masl metres below sea level

Monitors MW22-401 to MW22-408 was installed in April 2022; as such, water levels prior to this data are unavailable.

#### Table C-2: Groundwater Elevations in Mini-Piezometers

Monitor ID	Units	25-Sep-20	16-Nov-20	5-Apr-21	5-Jul-21	9-Sep-21	3-Nov-21	13-May-22	13-Jul-22	20-Sep-22	25-Nov-22	28-Mar-23	1-Nov-23	7-Mar-24
MP1-S	mbgs	n.d.	-0.09	-0.17	-0.26	-0.04	-0.05	-0.02	0.09	0.27	-0.06	-0.08	-	-0.05
	masl	n.d.	510.64	510.72	510.81	510.59	510.61	510.57	510.46	510.28	510.61	510.63	-	510.60
MP1-D	mbgs	n.d.	0.00	0.92	0.08	-0.19	-0.70	-0.04	0.78	0.86	0.25	-0.12	-	-0.23
	masl	n.d.	510.52	509.60	510.44	510.71	511.22	510.56	509.74	509.66	510.27	510.64	-	510.75

Notes:

mbgs metres below ground surface

masl metres below sea level

#### Table C-3: Vertical Hydraulic Gradients

Monitor ID	25-Sep-20	16-Nov-20	5-Apr-21	5-Jul-21	9-Sep-21	3-Nov-21	13-May-22	13-Jul-22	20-Sep-22	25-Nov-22	28-Mar-23	1-Nov-23	7-Mar-24
MP101													
Shallow monitor (masl)	-	510.64	510.72	510.81	510.59	510.61	510.57	510.46	510.28	510.61	510.63	-	510.60
Deep monitor (masl)	-	510.52	509.60	510.44	510.71	511.22	510.56	509.74	509.66	510.27	510.64	-	510.75
Hydraulic gradient (m/m)	-	0.11	-	0.33	-0.11	-0.55	0.01	0.65	0.56	0.31	0.00	-	-0.13
MW22-405													
Shallow monitor (masl)	-	-	-	-	-	-	511.25	510.26	509.51	510.24	512.02	512.02	511.97
Deep monitor (masl)	-	-	-	-	-	-	511.25	510.24	509.47	510.20	511.99	511.99	511.88
Hydraulic gradient (m/m)	-	-	-	-	-	-	0.00	0.00	0.01	0.01	0.01	0.01	0.02
BH-7													
Shallow monitor (masl)	511.82	512.08	512.05	511.95	512.06	512.09	-	511.62	511.35	512.02	512.06	512.02	512.04
Deep monitor (masl)	511.83	512.05	512.04	511.83	512.06	512.07	511.91	511.47	511.33	512.01	512.05	512.02	512.02
Hydraulic gradient (m/m)	0.00	0.01	0.00	0.03	0.00	0.00	-	0.03	0.00	0.00	0.00	0.00	0.00

Notes:

Positive hydraulic gradients indicates downward groundwater movement (i.e., recharge conditions)









# Appendix D Hydraulic Conductivity

#### Hydrogeological Assessment

Flato Ida

Flato Ida Dundalk Inc.

SLR Project No.: 209.30125.00001

May 6, 2024








## Appendix E MECP Water Well Records

## Hydrogeological Assessment

Flato Ida

Flato Ida Dundalk Inc.

SLR Project No.: 209.30125.00001

May 6, 2024



## Table E-1: MECP Water Well Record Summary

WELL ID	TAG	DATE COMPLETED	DEPTH (M)	BOTTOM LITHOLOGY	STATUS	WATER USE	DEPTH WATER FOUND (M)	STATIC LEVEL (M)	PUMPING RATE (LPS)
2500875		4/1/1953	112.5	ROCK	Water Supply	Public	112.5	5.5	1.137
2500899		1/14/1967	18.3	GRAVEL	Water Supply	Domestic	18.3	1.8	1.137
2502018		8/20/1952	34.1	SHALE	Water Supply	Livestock	34.1	3.4	1.895
2503762		5/12/1972	37.8	ROCK	Water Supply	Domestic	35.1	6.1	0.606
2504542		3/6/1974	28	ROCK	Water Supply	Livestock	27.4	2.4	1.516
2505043		3/18/1975	86.9	ROCK	Water Supply	Municipal	34.7	7.9	13.568
2506106		6/28/1977	71.3	LIMESTONE	Water Supply	Domestic	54.9	12.5	0.455
2506130		7/7/1977	32	LIMESTONE	Water Supply	Domestic	31.1	6.4	2.274
2506305		11/14/1977	30.2	LIMESTONE	Water Supply	Domestic	29.6	3.4	1.895
2506846		3/24/1979	51.8	LIMESTONE	Water Supply	Domestic	51.8	9.1	0.455
2508036		11/21/1983	42.7	LIMESTONE	Water Supply	Domestic	42.7	8.2	0.379
2508359		8/6/1984	70.1	LIMESTONE	Water Supply	Domestic	68.6	10.7	0.758
2509298		8/29/1987	74.4	LIMESTONE	Water Supply	Domestic	74.4	11.9	0.379
2509474		7/12/1988	52.7	LIMESTONE	Water Supply	Domestic	52.7	11.3	0.379
2509476		6/2/1988	30.8	LIMESTONE	Water Supply	Domestic	30.8	8.5	0.91
2512662		9/22/1994	36.9	LIMESTONE	Water Supply	Public	29.3	7.3	0.758
2513366		9/12/1997	55.5	LIMESTONE	Water Supply	Domestic	35.1	15.2	0.303
2513888		5/31/1999	25.9	LIMESTONE	Water Supply	Domestic	25.3	4.6	0.606
2514390		8/22/2000	37.2	LIMESTONE	Water Supply	Domestic	24.1	6.7	0.531
2515539		6/9/2003	35.7	LIMESTONE	Water Supply	Domestic	27.4	6.1	4.548
2516266	A011038	10/23/2004	5.5	TILL	Observation Wells				
2516764	A030200	10/13/2005	48.8	LIMESTONE	Water Supply	Domestic	48.8	15.2	0.758
7119170	A073231	10/28/2008	35.4	LIMESTONE	Water Supply	Public	29.0	5.2	4.548
7140441		2/7/2010	0		Abandoned-Other	Other		0.8	
7140446		2/7/2010	0		Abandoned-Other	Other		0.7	
7140450		2/7/2010	0		Abandoned-Other			0.6	
7140452		2/1/2010	0		Abandoned-Other	Other		1	
7224832	A134613	6/26/2014	6.1	SAND	Observation Wells	Monitoring	3.0		
7285238	A210321	11/17/2016	7.6	CLAY	Observation Wells	Monitoring	4.0		
7332812	A161132	7/20/2018	6.1	SILT	Monitoring and Test Hole	Monitoring			
7332813	A237960	7/20/2018	4.6	SILT		Monitoring			
7332814	A241019	7/20/2018	6.1	SILT	Monitoring and Test Hole	Monitoring			
7333654	A250373	5/16/2019	0		Water Supply	Domestic		2.3	1.137
7426721	A347533	4/18/2022	4.6	SILT	Test Hole	Monitoring			
7426723	A347544	4/18/2022	6.1	SILT	Test Hole	Monitoring	5.3		
7426726	A347545	4/18/2022	6.1	SILT	Test Hole	Monitoring	5.3		
7426727	A347562	4/18/2022	6.1	SILT	Test Hole	Monitoring	1.5		
7426728	A347565	4/18/2022	10.7	SILT	Test Hole	Monitoring	5.3		
7426729	A347532	4/15/2022	6.1	SILT	Observation Wells	Monitoring	1.5		
7426730	A347543	4/18/2022	6.1	SILT	Test Hole	Monitoring	5.3		
7426731	A347559	4/18/2022	6.1	SILT	Test Hole	Monitoring	5.3		
7426732	A347564	4/18/2022	6.1	SILT	Observation Wells	Monitoring	1.5		
7426733	A347558	4/18/2022	6.1	SILT	Test Hole	Monitoring			

WELL ID	LAYER	FORMATION	FORMATION END DEPTH (M)	
	1	CLAY	24.38	
2500875	2	GRAVEL	31.09	
	3	ROCK	112.47	
	1	TOPSOIL	0.30	
2500899	2	HARDPAN	15.24	
	3	GRAVEL	18.29	
	1	TOPSOIL	0.91	
	2	HARDPAN	24.38	
2502018	3	MEDIUM SAND	26.82	
	4	LIMESTONE	33.53	
	5	SHALE	34.14	
	1	TOPSOIL	0.61	
	2	HARDPAN	7.62	
2503762	3	HARDPAN	25.91	
2000102	4	SAND	30.48	
	5	ROCK	37.80	
	1	TOPSOIL	0.91	
	2		10.67	
2504542	2		24.29	
2004042	3		24.30	
		GRAVEL	27.43	
	5	RUCK	20.04	
	1	TUPSUIL	0.61	
	2	HARDPAN	8.53	
	3	HARDPAN	23.47	
2505043	4	CLAY	28.04	
	5	ROCK	34.75	
	6	ROCK	44.20	
	7	ROCK	57.91	
	8	ROCK	86.87	
	1	TOPSOIL	0.30	
	2	CLAY	7.01	
	3	HARDPAN	37.19	
	4	LIMESTONE	39.32	
2506106	5	LIMESTONE	46.94	
2000100	6	LIMESTONE	51.21	
	7	LIMESTONE	53.95	
	8	LIMESTONE	65.53	
	9	SANDSTONE	67.97	
	10	LIMESTONE	71.32	
	1	GRAVEL	8.23	
2506130	2	HARDPAN	29.57	
	3	LIMESTONE	32.00	
	1	TOPSOIL	0.61	
0500005	2	CLAY	9.14	
			27/3	
2506305	3	HARDPAN	21.40	
2506305	3	LIMESTONE	30.18	
2506305	3 4 1		30.18 0.61	
2506305	3 4 1 2	LIMESTONE TOPSOIL CLAY	30.18 0.61 3.35	
2506305	3 4 1 2 3	LIMESTONE TOPSOIL CLAY HARDPAN	30.18 0.61 3.35 35.97	

## Table E-2: MECP Water Well Record Formations

	1	CLAY	7.32	
2508026	2	HARDPAN	15.54	
2506050	3	GRAVEL	31.39	
	4	LIMESTONE	42.67	
2508359	1	TOPSOIL	0.30	
	2	CLAY	9.14	
	3	HARDPAN	33.53	
	4	LIMESTONE	57.30	
	5	LIMESTONE	70.10	
	1	TOPSOIL	0.30	
	2	CLAY	4.27	
2509298	3	CLAY	22.25	
	4	HARDPAN	34.75	
	5	LIMESTONE	74.37	
2509474	1	TOPSOIL	0.30	
	2	CLAY	8.53	
	3	HARDPAN	23.77	
	4	LIMESTONE	52.73	

CLAY

WELL ID	LAYER	FORMATION	FORMATION END		
	1	CLAY	8 53		
2509476	2	HARDPAN	28.04		
	3	LIMESTONE	30.78		
	1	CLAY	2.74		
	2	BOULDERS	3.96		
2512662	3	HARDPAN	24.69		
	4	LIMESTONE	36.88		
	1	CLAY	7.62		
2513366	2	HARDPAN	28.96		
	3	LIMESTONE	55.47		
	1	CLAY	6.71		
2513888	2	CLAY	23.16		
	3	LIMESTONE	25.91		
	1	CLAY	19.81		
2514390	2	LIMESTONE	37.19		
	1	CLAY	3 35		
	2	SILT	13 72		
2515539	3	CLAY	23.47		
	4		35.66		
	1	EIMEOTONE	4 57		
2516266	2	ТШІ	5.49		
	1	FILL	0.40		
2516764	2 2		25.07		
2010/04	2		10.91 10.77		
	1		40.77		
			0.01		
7119170	2		25.20		
	3		25.30		
7440444	4	LIMESTONE	35.30		
7140441					
/140446					
7140450					
7140452					
7224832	1	TOPSOIL	3.05		
	2	SAND	6.10		
	1	SAND	4.57		
7285238	2	SAND	6.10		
	3	CLAY	7.62		
	1				
7332812	2	GRAVEL	1.83		
	3	SILT	6.10		
	1				
7332813	2	GRAVEL	1.83		
	3	SILT	4.57		
	1				
7332814	2	GRAVEL	1.83		
	3	SILT	6.10		
7333654					
7426721	1	TOPSOIL	1.52		
	2	SILT	4.57		
7426722	1	FILL	0.76		
1720120	2	SILT	6.10		
7/26726	1	FILL	0.76		
1720120	2	SILT	6.10		
7426727	1	TOPSOIL	1.52		
1720121	2	SILT	6.10		
7/06700	1	TOPSOIL	1.52		
1420120	2	SILT	10.67		
7406700	1	TOPSOIL	1.52		
1420129	2	SILT	6.10		
7400700	1	FILL	1.52		
1426730	2	SILT	6.10		
7/00-0	1	FILL	0.91		
/426731	2	SILT	6.10		
	1	TOPSOII	1 52		
7426732	2	SILT	6 10		
	1	FILI	1.52		
7426733	2	SII T	6 10		
	~		0.10		



Making Sustainability Happen